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- Health and Safety Context
- LES/DES/SAS Quality
 - Grid Resolution
- Application
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LES in Health and Safety

- Fire Dynamics Simulator (FDS) from NIST



- Used extensively in fire investigation, e.g. collapse of World Trade Center twin towers
- OECD Best Practice Guidelines for CFD in Nuclear Reactor Safety Applications:

“Obviously, more advanced scale-resolving CFD methods based on LES, DES, or SAS are required for such cases.”


LES/DES/SAS Quality Issues



Differences compared to RANS quality issues:

- Subgrid-scale model
- Wall treatment
- Unsteady inflow conditions
- Numerical schemes
- Grid dependence ←
- Temporal treatment

Grid Resolution

- Complex issue: dynamic interaction of model and discretization errors
- In the limit:
 - Overly coarse grids produce poor results
 - Very fine grid, LES results tend to DNS
- What practical guidance exists on grid resolution?
 1. Rules of thumb  e.g. 20 cells across characteristic fire diameter
 2. Measures based on prior RANS
 3. Single-grid estimators
 4. Multi-grid estimators

2. Measures based on RANS

- Ratio of integral turbulence length scale to grid cell size:
$$\frac{(k^{3/2} / \varepsilon)}{\Delta} > 10$$

- Ratio of grid cell size to Kolmogorov length scale:
$$\frac{\Delta}{\eta} = \frac{\Delta}{(v^3 / \varepsilon)^{1/4}} < 25$$

- Near-wall spacing, for wall-resolving LES:

$$(x^+, y^+, z^+) < (100, 2, 20)$$

“Young person’s guide to DES Grids”, Spalart 2001

3. Single-grid estimators

- Viscosity ratio, $\nu_{eff}/\nu < 20$ for $Re_t \sim 1200$
 < 5 for $Re_t \sim 300$
- Relative effective viscosity index
- Subgrid activity parameter
- Proportion of resolved turbulent kinetic energy:

$$\frac{k_{res}}{k_{res} + k_{sgs} + k_{num}} > 0.8$$

- Power spectral density (-5/3 slope)

4. Multi-grid estimators

- “Index of Quality” of Celik *et al.* (2005)
- Grid and Model variation of Klein (2005)
- Both based on Richardson extrapolation using multiple LES solutions

Known Limitations

- Accuracy of RANS model, esp. in transitional or massively separated flows.
- Subgrid activity parameter close to 1.0 in most industrial LES
- Resolved TKE can be higher on coarse grid than on fine grid
- Magnitude of numerical dissipation?
- Multi-grid methods: resolution not in asymptotic range for RE , interaction of errors
- Spectra: modified by buoyancy, only found at points and in low- Re flows?

Application



Continuous methane gas release in a ventilated room

Interest: to predict the flammable gas cloud size

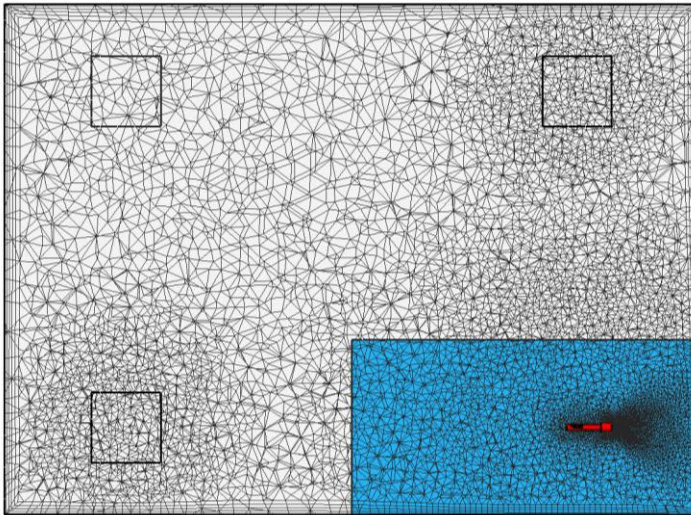


Flow Behaviour

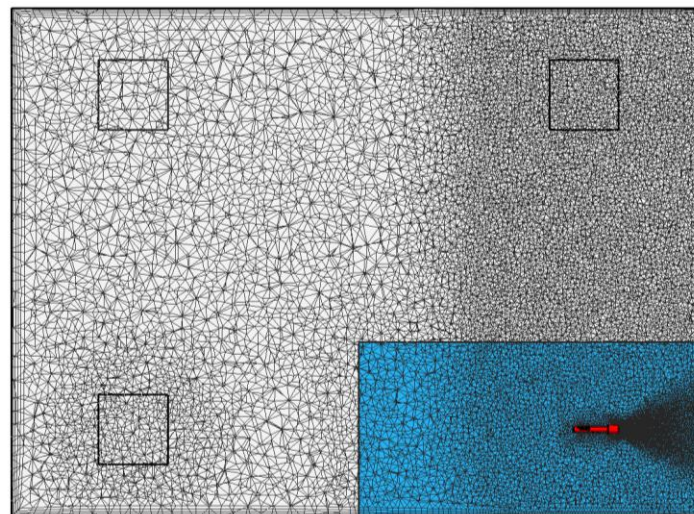
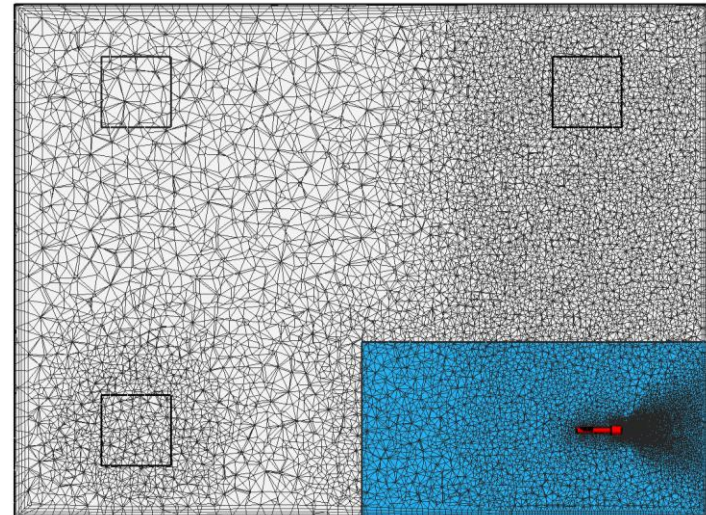


Grids

Coarse (0.2M nodes)

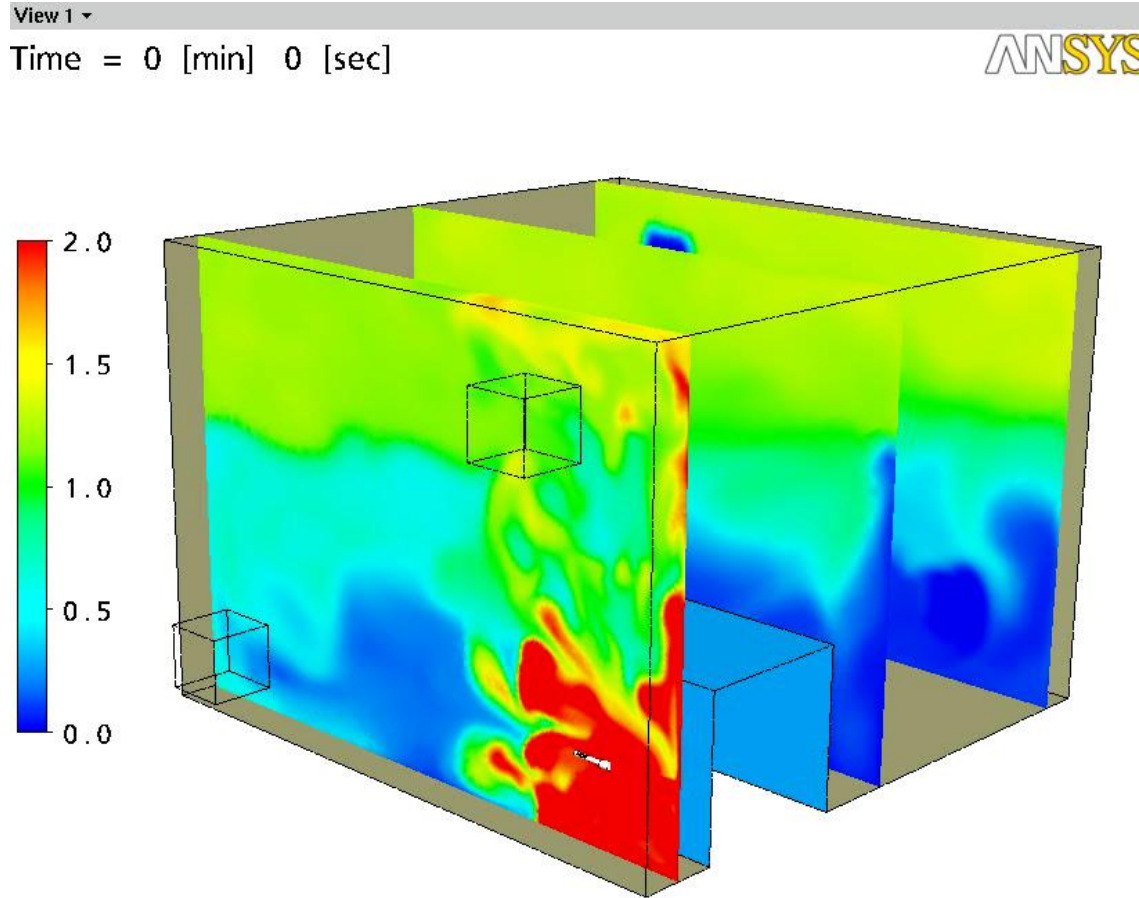


Medium (0.4M nodes)



Fine
(0.7M nodes)

Gas Cloud

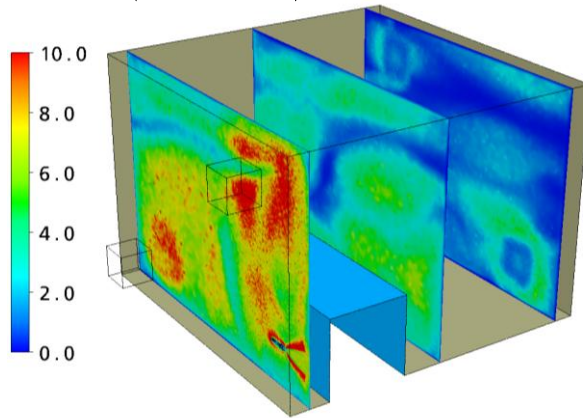


	Timescale (s)
Gas jet	10^{-5}
Vent inlet	2 – 3
Plume	3
Air change	300

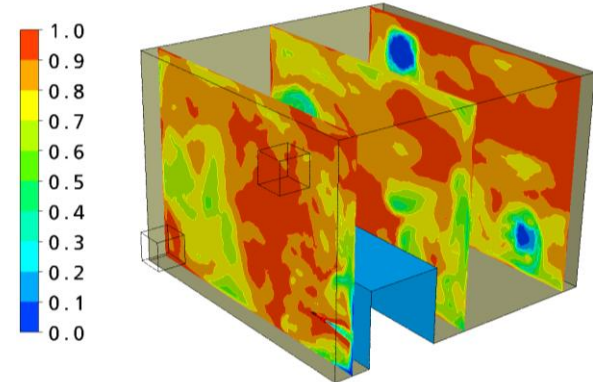
- Time-step $\Delta t = 0.1$ s
- Averaging period ≈ 7 mins

Grid Resolution

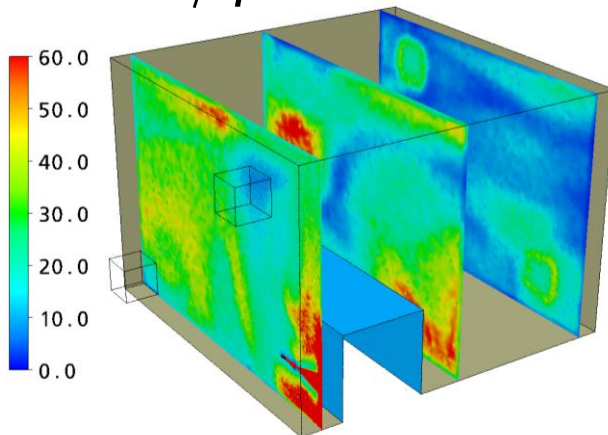
$$(k^{3/2} / \varepsilon) / \Delta > 10$$



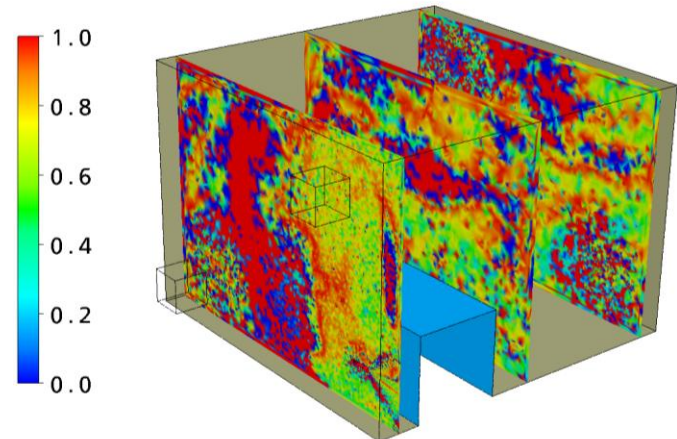
$$k_{res} / (k_{res} + k_{sgs}) > 0.8$$



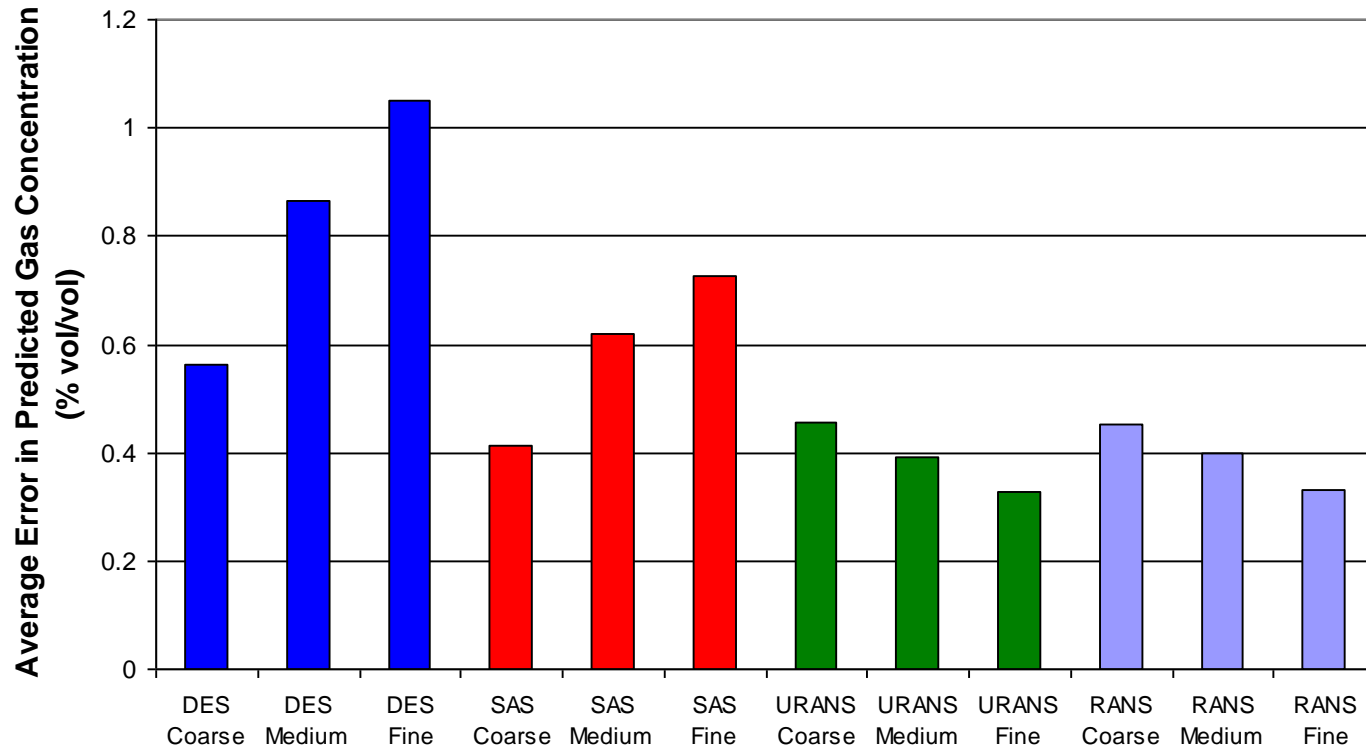
$$\Delta / \eta < 25$$



$$LES_IQ_k > 0.8$$

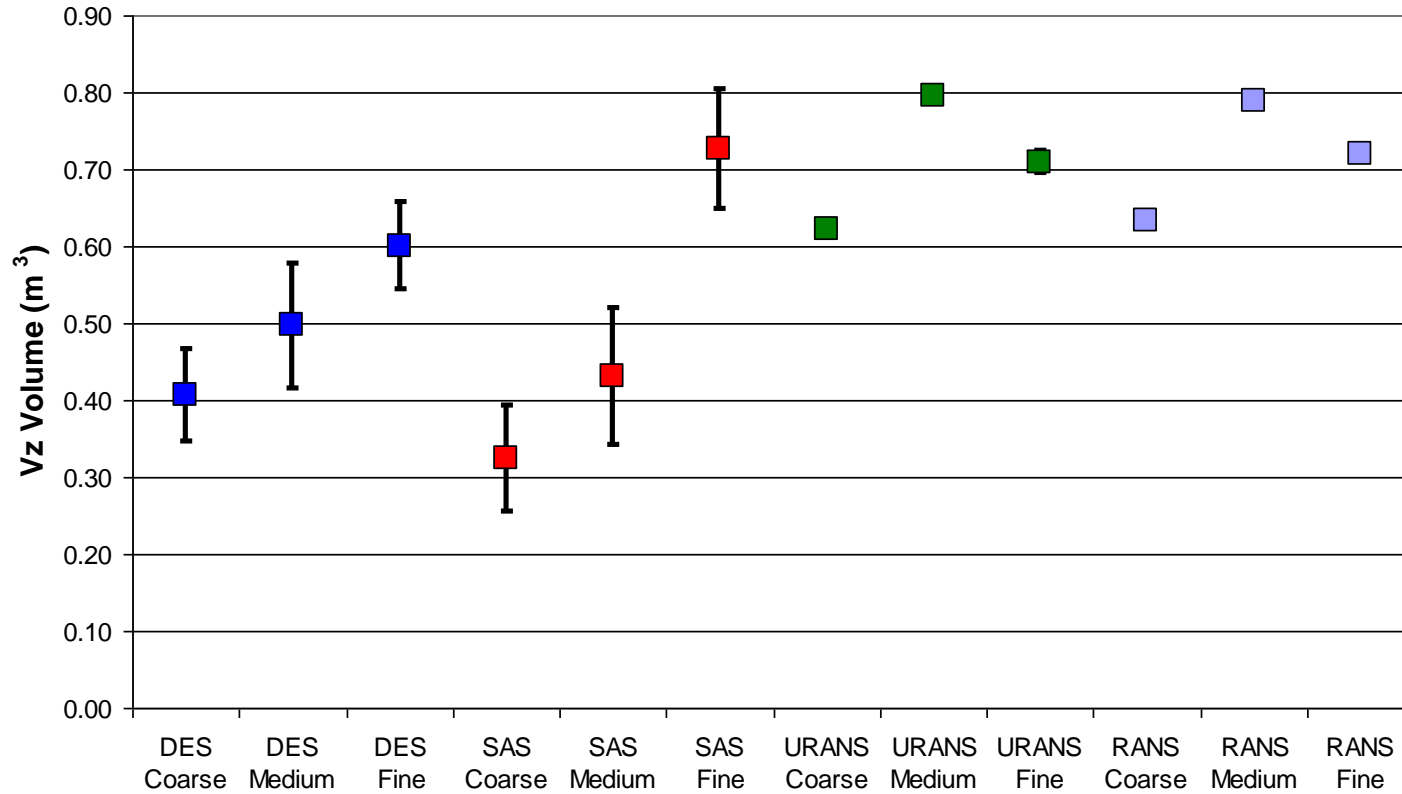


Results



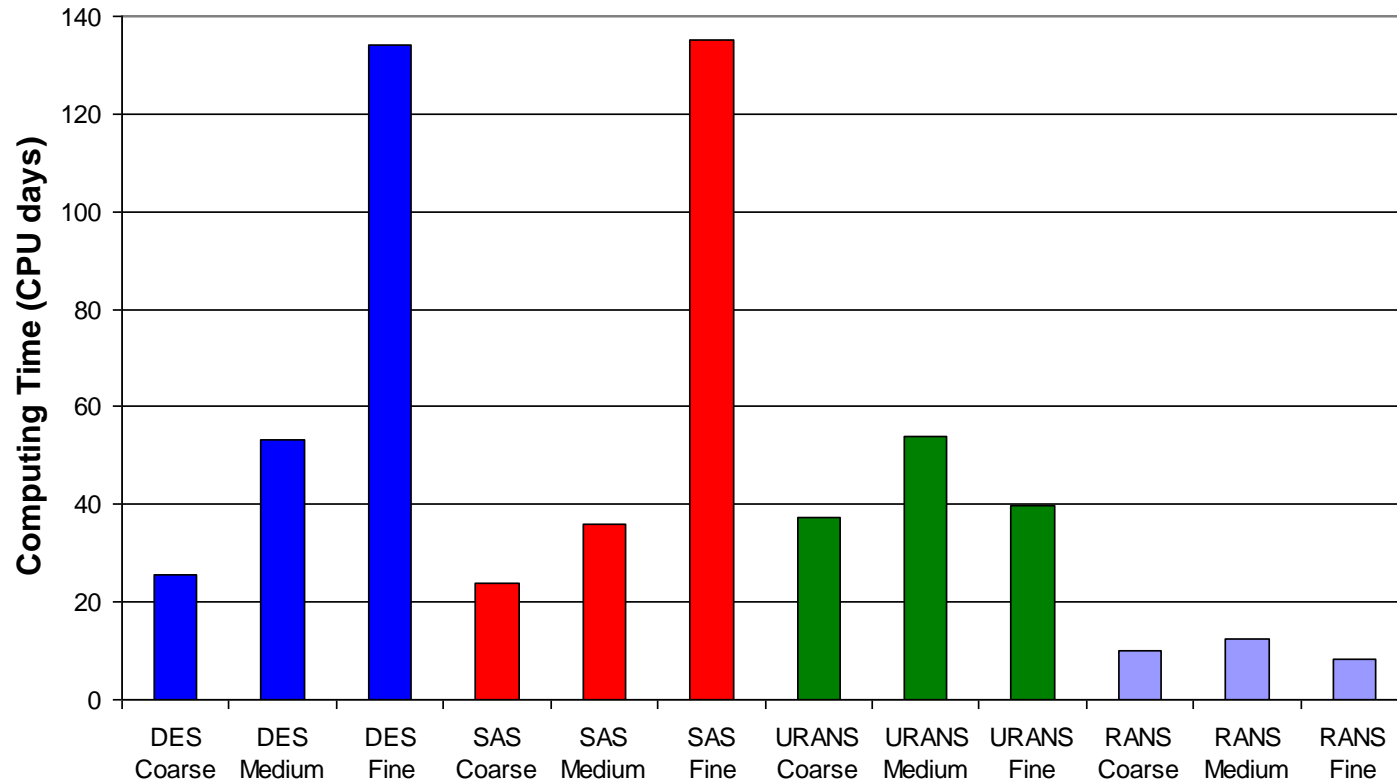
Average error between CFD and experiments

Results



Predicted mean gas cloud size and 95% confidence intervals

Computing Time



Computing time in CPU days

Conclusions

- Number of grid resolution indices in literature.
- Each has advantages/limitations, none ideal.
- Results for test case show that DES/SAS can be worse than SST if grid resolution marginal.
- SAS appears sensitive to grid resolution.
- Confidence Intervals useful to identify statistical uncertainty and define duration of simulation.
- Further research in LES/DES/SAS/URANS quality and trust required: cohort studies?
- Suggestion: document grid resolution and statistical uncertainty in future results.

Acknowledgements

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 - Andrew Patton (Oxford)
 - Raf Theunissen (VKI)
 - M. L. Riethmuller (VKI)
 - Adrian Kelsey (HSL)
- } for assistance with bootstrapping

Questions?






HEALTH & SAFETY
LABORATORY

DES Blending Function

Turbulence Model

$$\varepsilon = \beta^* k \omega F_{DES}$$

$$F_{DES} = \max \left[\frac{k^{3/2} / \varepsilon}{C_{DES} \Delta} (1 - F_{SST}), 1 \right]$$


Set to zero to recover Strelets
(2001) model

$$C_{DES} = 0.61$$

Discretization Scheme

$$\varphi_{ip} = \sigma \varphi_{ip,U} + (1 - \sigma) \varphi_{ip,C}$$

$$\sigma = \tanh(A^3)$$

$$A = \max \left(\frac{C_{DES} \Delta_{\max}}{L_{turb} g} - 0.5, 0 \right)$$

$$L_{turb} = \frac{\sqrt{k}}{c_{\mu} \omega}$$

$$g = \max \left[\tanh(B^4), 10^{-10} \right]$$

$$B = 2\Omega \frac{\max(S, \Omega)}{\max \left(\frac{S^2 + \Omega^2}{2}, 10^{-10} \right)}$$

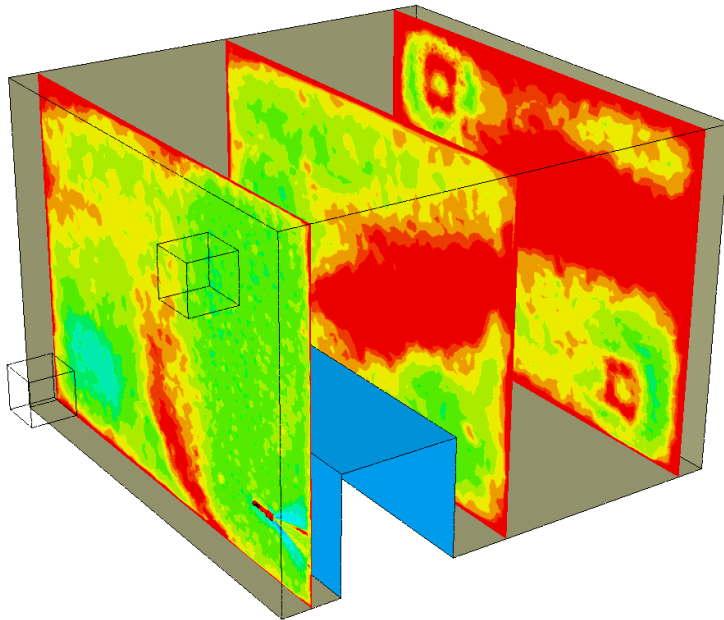
$$\sigma^{\lim} = \max \left[\sigma, 1 - \min \left(\frac{5}{CFL}, 1 \right) \right]$$

DES Blending Function

Turbulence Model

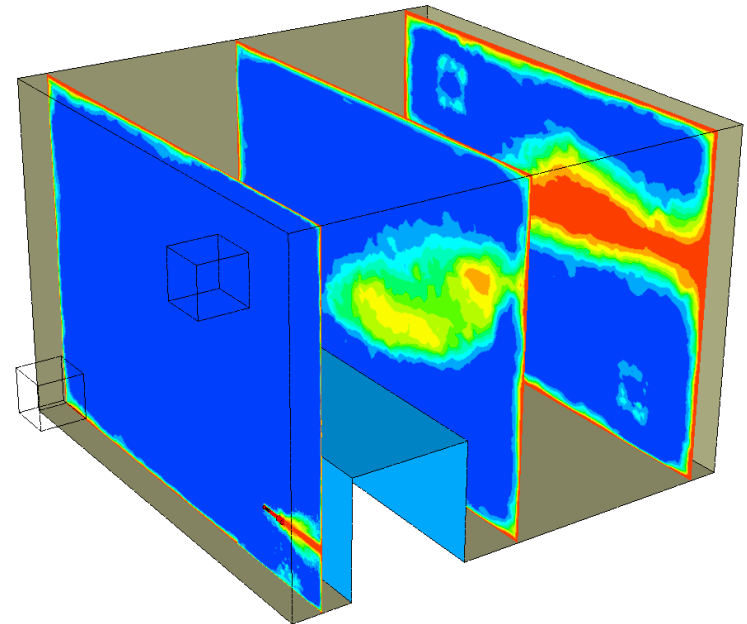
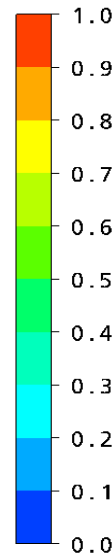
1 = RANS ; <1 = DES

$$(C_{DES} \Delta) / (k^{3/2} / \varepsilon)$$

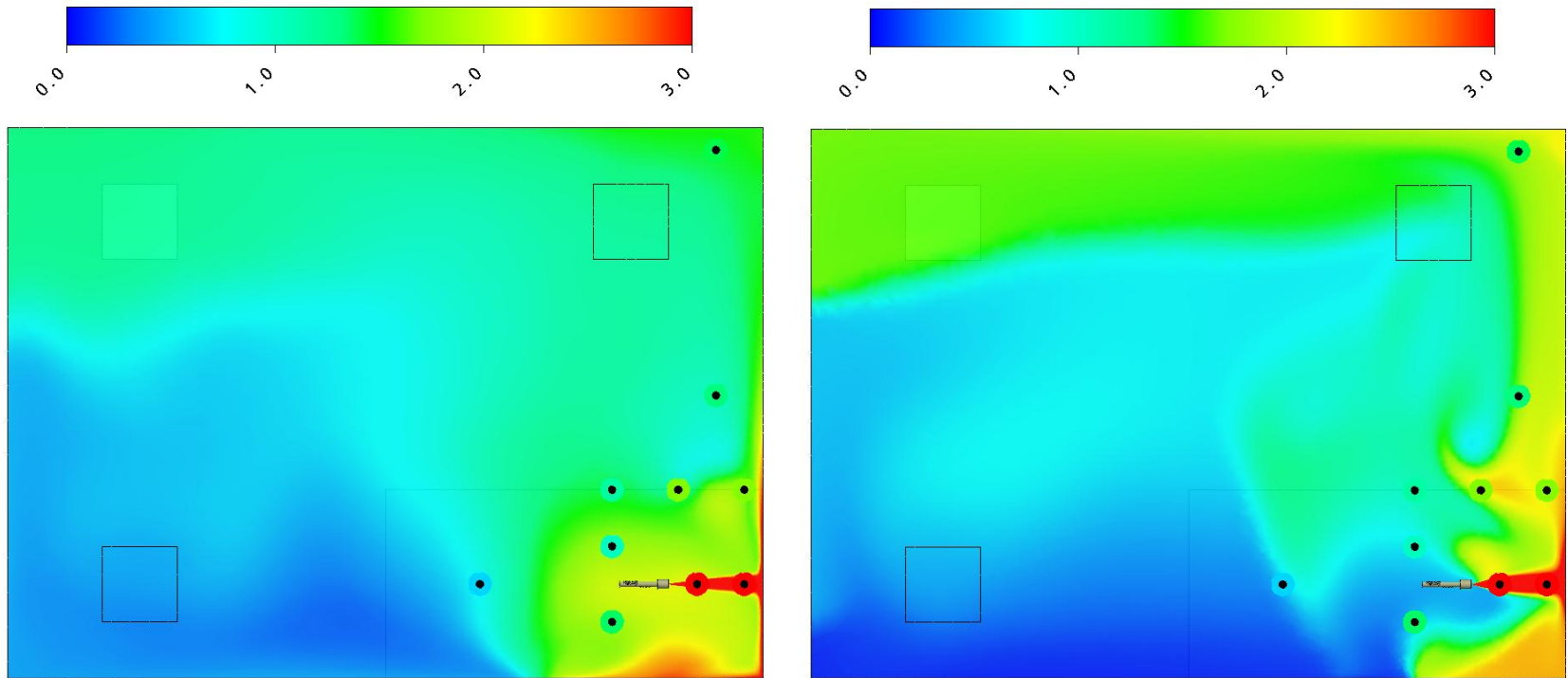


Discretization Scheme

0 = central ; 1 = upwind-biased



Results

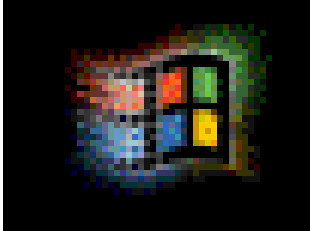


DES

RANS (SST)

Mean Gas Concentrations (% vol/vol)

Results



LES “Index of Quality”

$$LES_IQ_k = 1 - \frac{|k_{tot} - k_{res}|}{k_{tot}}$$

$$k_{tot} = k_{res} + a_k h^p$$

← $p=2$
Cell size

$$a_k = \frac{(k_{res})_1 - (k_{res})_2}{h_2^2 - h_1^2}$$

Subscript: 1= Medium, 2 = fine

Problems when:

$$\underline{(k_{res})_1 > (k_{res})_2}$$

$$\rightarrow a_k < 0$$

$$\rightarrow k_{res} + a_k h^p < | a_k h^p |$$

$$\rightarrow \frac{|k_{tot} - k_{res}|}{k_{tot}} > 1$$

$$\rightarrow LES_IQ_k < 0$$

or when:

$$\underline{(k_{res})_1 \gg (k_{res})_2}$$

$$\rightarrow a_k \ll 0$$

$$\rightarrow k_{tot} < 0$$

$$\rightarrow LES_IQ_k > 1$$

2. Measures based on RANS

- Ratio of integral turbulence length scale to grid cell size:

$$\frac{(k^{3/2} / \varepsilon)}{\Delta}$$

Baggett <i>et al.</i> (1997)	Channel flow	3.5
Jiménez & Moser (1998)	Channel flow	3.5 – 7
Pope (2000)	High- <i>Re</i> isotropic turbulence	12 – 17
Addad <i>et al.</i> (2004)	Buoyancy opposed wall jet	12 – 30
Van Maele & Merci (2008)	Tunnel fires	12

2. Measures based on RANS

- Ratio of grid cell size to Kolmogorov length scale

$$\frac{\Delta}{\eta} = \frac{\Delta}{\left(\nu^3 / \varepsilon\right)^{1/4}}$$

Celik <i>et al.</i> (2005)	Rule of thumb	< 25
Hadžiabdić & Hanjalić (2008)	Impinging Jet	< 21

3. Single-grid estimators

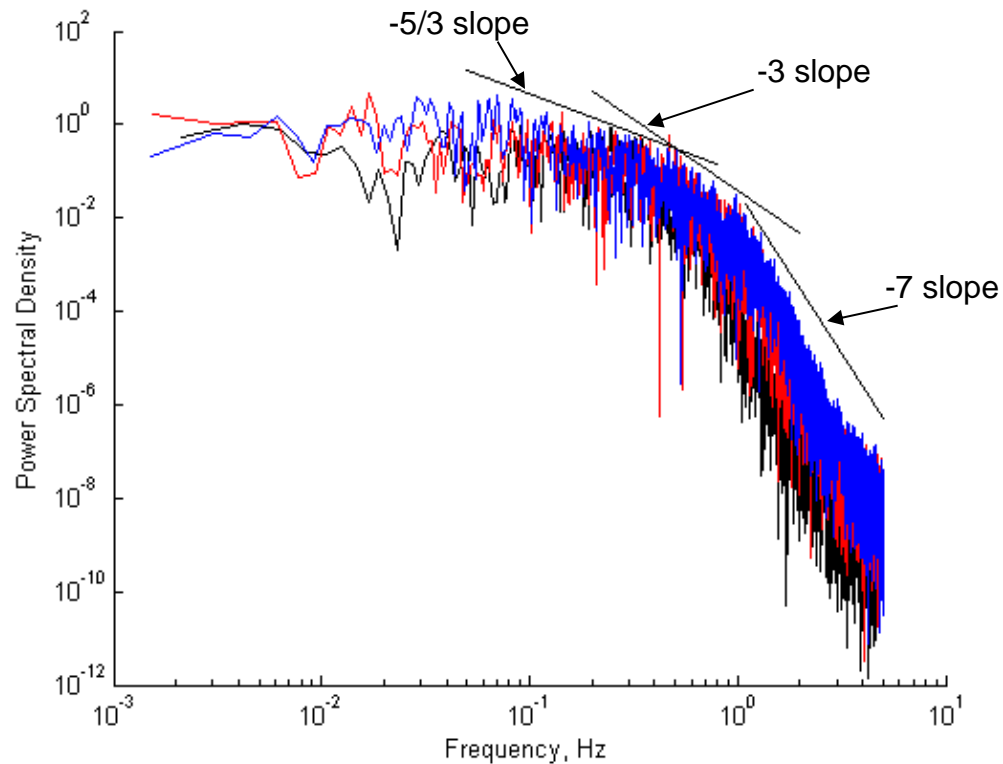
- Subgrid activity parameter

(Geurts & Fröhlich, 2002)

$$S = \frac{\overline{\varepsilon_t}}{\overline{\varepsilon_t + \varepsilon_\mu}} = \frac{\overline{\nu_t S^2}}{(\nu + \overline{\nu_t}) S^2} \quad \begin{array}{l} = 0 \text{ for DNS} \\ = 1 \text{ for high-}Re \text{ LES} \end{array}$$

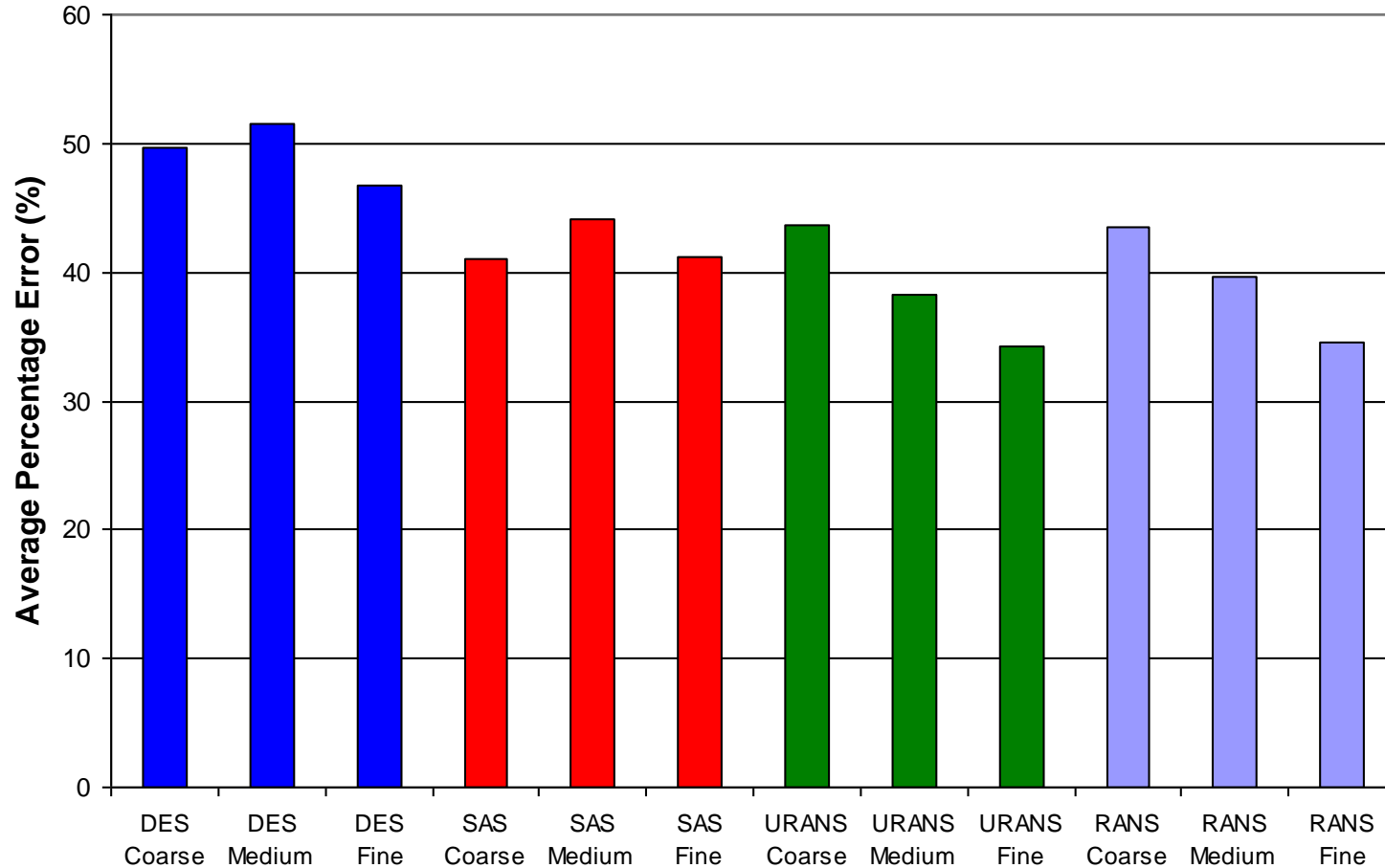
3. Single-grid estimators

Power spectral density based on concentration fluctuations



DES results: – coarse, – medium, – fine

Error in Percentage Terms



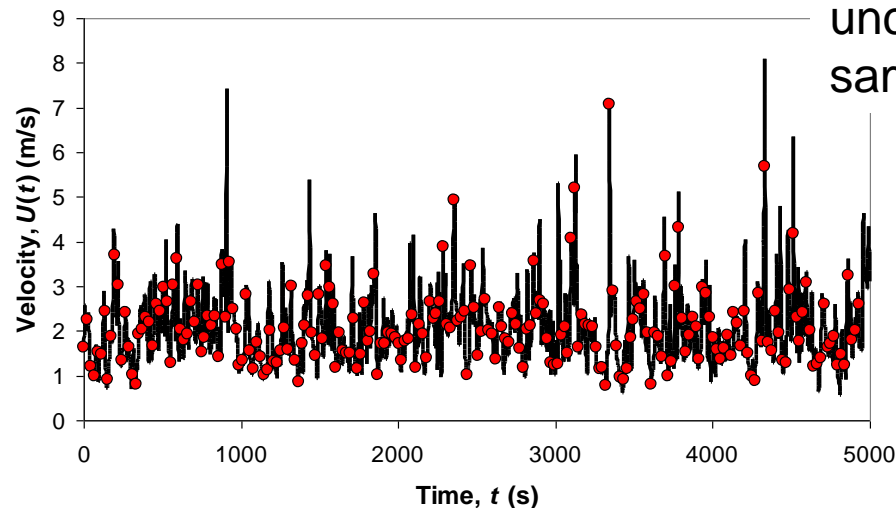
Statistical Uncertainty

- How long should the LES calculation be continued?
- Assess uncertainty in mean values using Confidence Intervals
- “95% confident that mean lies between x and y m/s”
- Fractional error:

$$e_s = \frac{k\sqrt{u^2/n}}{U}$$

Variance

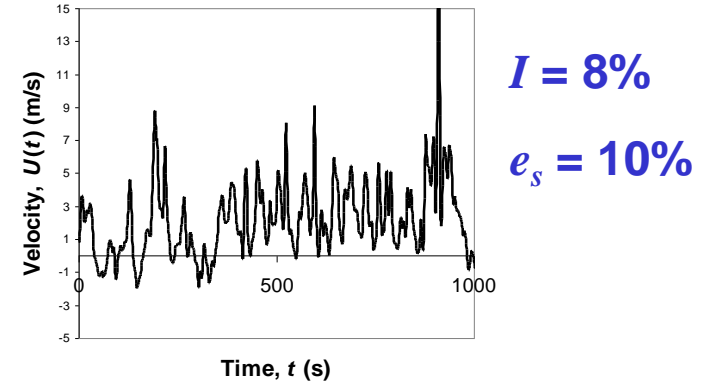
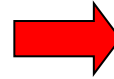
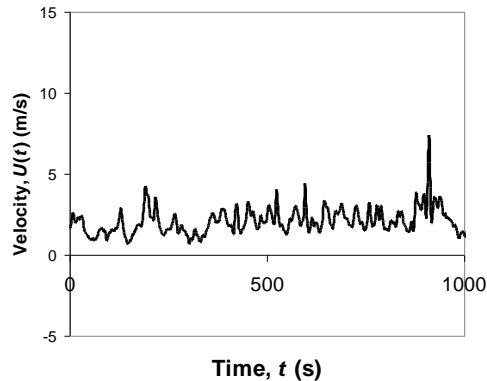
Number of uncorrelated samples



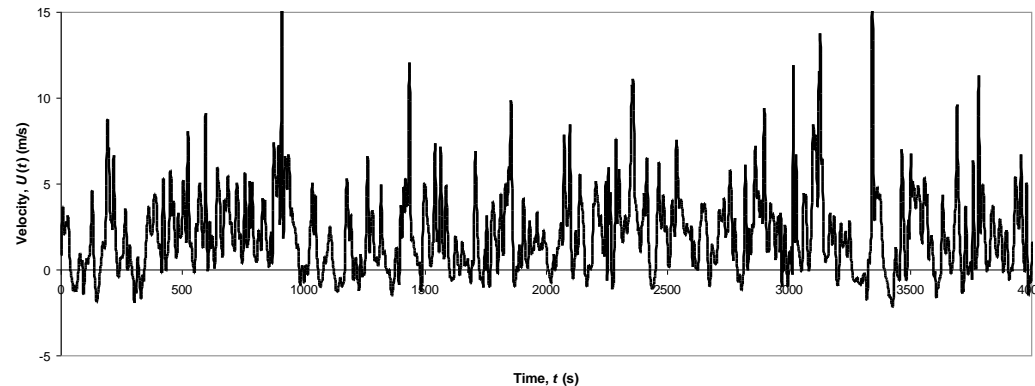
— velocity signal • uncorrelated samples

Statistical Uncertainty

- If the turbulence intensity $I = \sqrt{u^2} / U$ doubles:



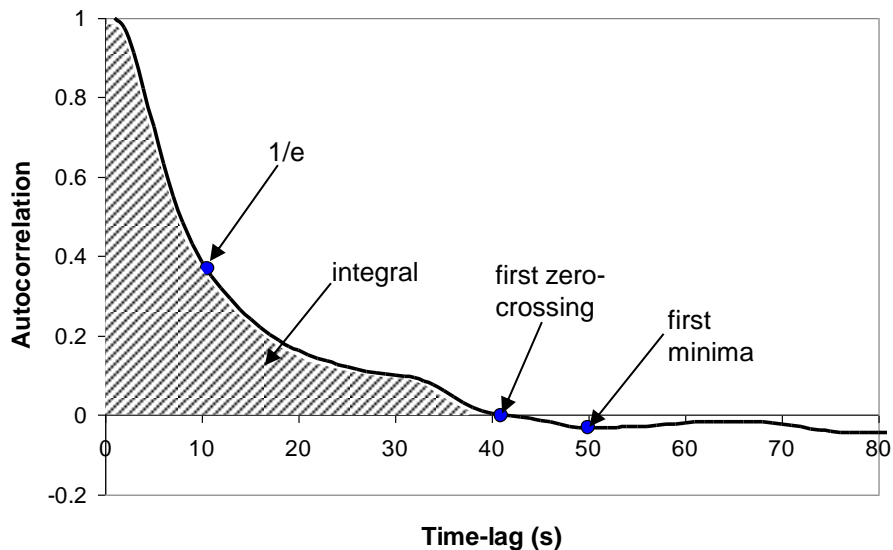
- Need to increase number of samples by factor of 4 to maintain same confidence level.



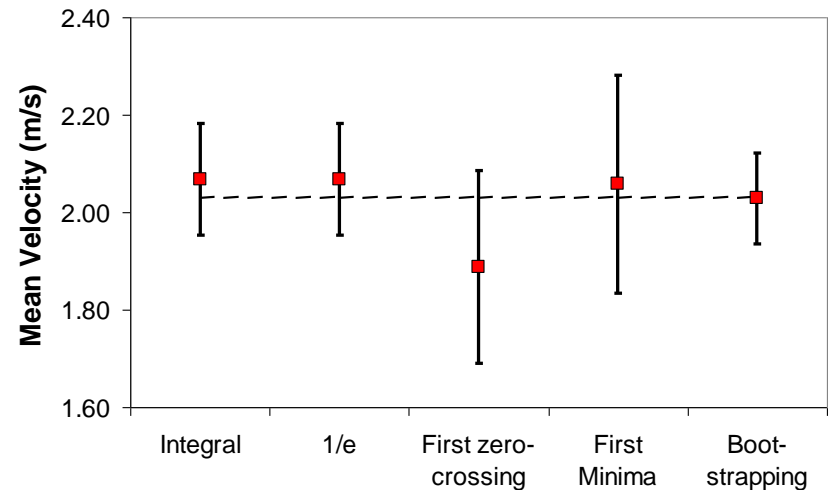
Statistical Uncertainty

- Classical approaches to calculate CI rely on *uncorrelated* data
 - Problem: need to sample signal at intervals spaced τ apart
 - How to calculate τ ? Various approaches possible which produce different e_s
- Alternative: *bootstrapping*
 - Can handle correlated data
 - Automatic block length selector means no user-defined parameters
 - Can also be used to calculate confidence intervals on Reynolds stresses etc.

Confidence Intervals



	Interval (s)	Mean \pm 95% CI
All data	-	2.03 \pm ?
Integral	22	2.06 \pm 2.8%
1/e	22	2.06 \pm 2.8%
First zero	82	1.90 \pm 5.2%
First min	100	2.06 \pm 5.4%
Bootstrap	-	2.03 \pm 2.3%



Bootstrapping

- Theunissen, R., A. Di Sante, M.L. Riethmuller, and R.A. Van den Braembussche, *Confidence estimation using dependent circular block bootstrapping: application to the statistical analysis of PIV measurements*. Exp. Fluids, 2008. **44**: p. 591-596.
- Garcia, C.M., P.R. Hackson, and M.H. Garcia, *Confidence intervals in the determination of turbulence parameters*. Exp. Fluids, 2006. **40**: p. 514-522.
- Wilks, D.S., *Statistical methods in the atmospheric sciences*. 2nd ed. 2006: Academic Press, Elsevier.
- Politis, D.N. and H. White, *Automatic block-length selection for the dependent bootstrap*. Econometric Reviews, 2004. **23**(1): p. 53-70.
- Patton, A., D.N. Politis, and H. White, *Correction to "Automatic block-length selection for the dependent bootstrap" by D. Politis and H. White*. Submitted for publication, 2008
(<http://www.economics.ox.ac.uk/members/andrew.patton>)