



Sensitivity and uncertainty analysis of consequence models

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30th November and 1st December 2016

Outline

- Background
- Sensitivity analysis of models
 - Local
 - Global
- Examples
- Conclusions
- Future directions

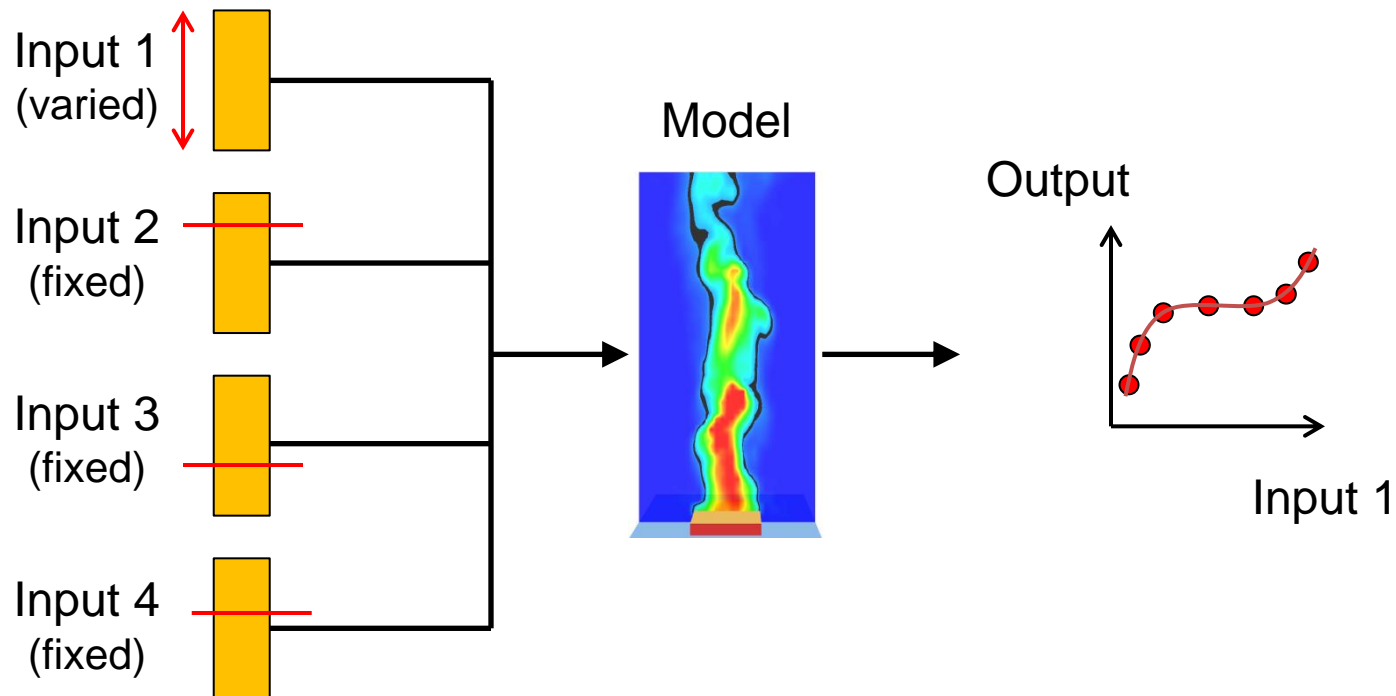
Background

- Consequence models for gas dispersion/fires/explosions have inputs which are often uncertain
 - e.g. gas pressure, hole size, wind speed
- Useful to know:
 - Which inputs have a significant effect on the results
 - How the model results change as the inputs change
 - What combination of inputs gives the worst-case consequence
- Benefits:
 - Prioritise efforts on the most sensitive inputs
 - Improved understanding of the problem



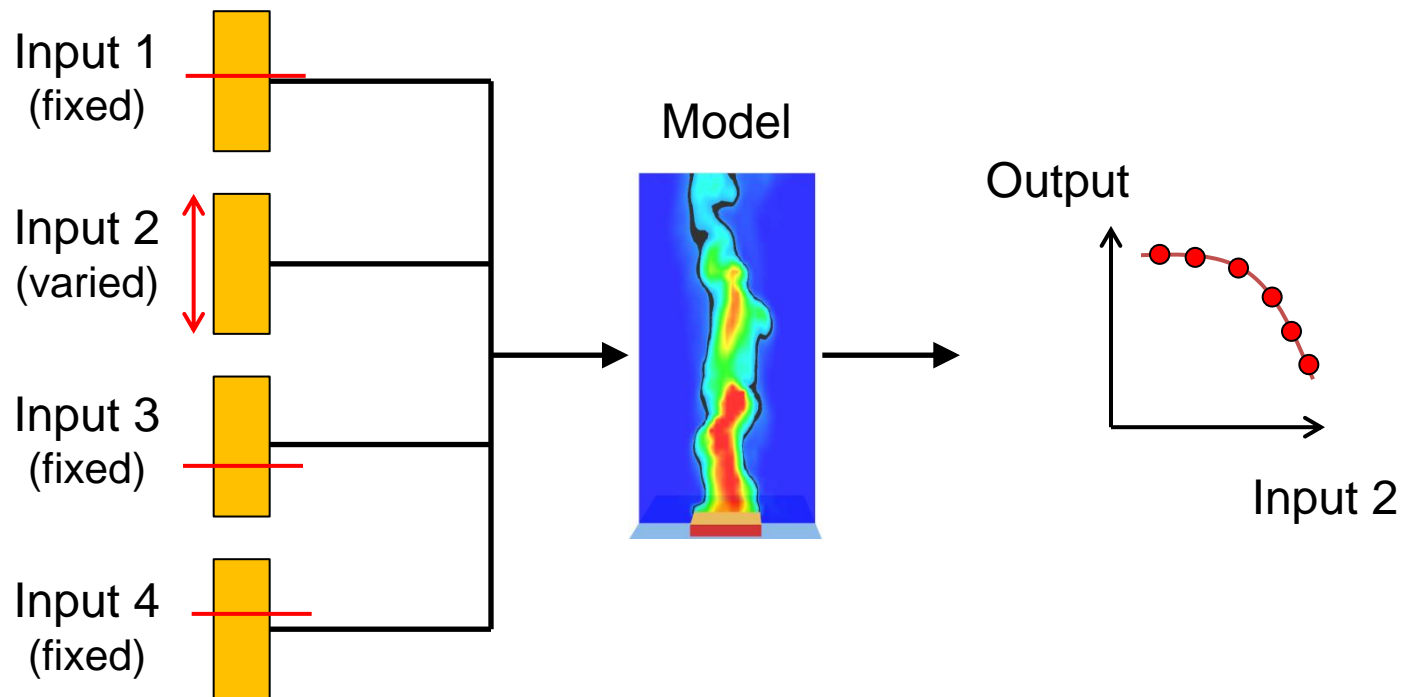
Sensitivity Analysis

- Two approaches for sensitivity analysis:
 1. **Local:** vary one parameter at a time from a “baseline” case



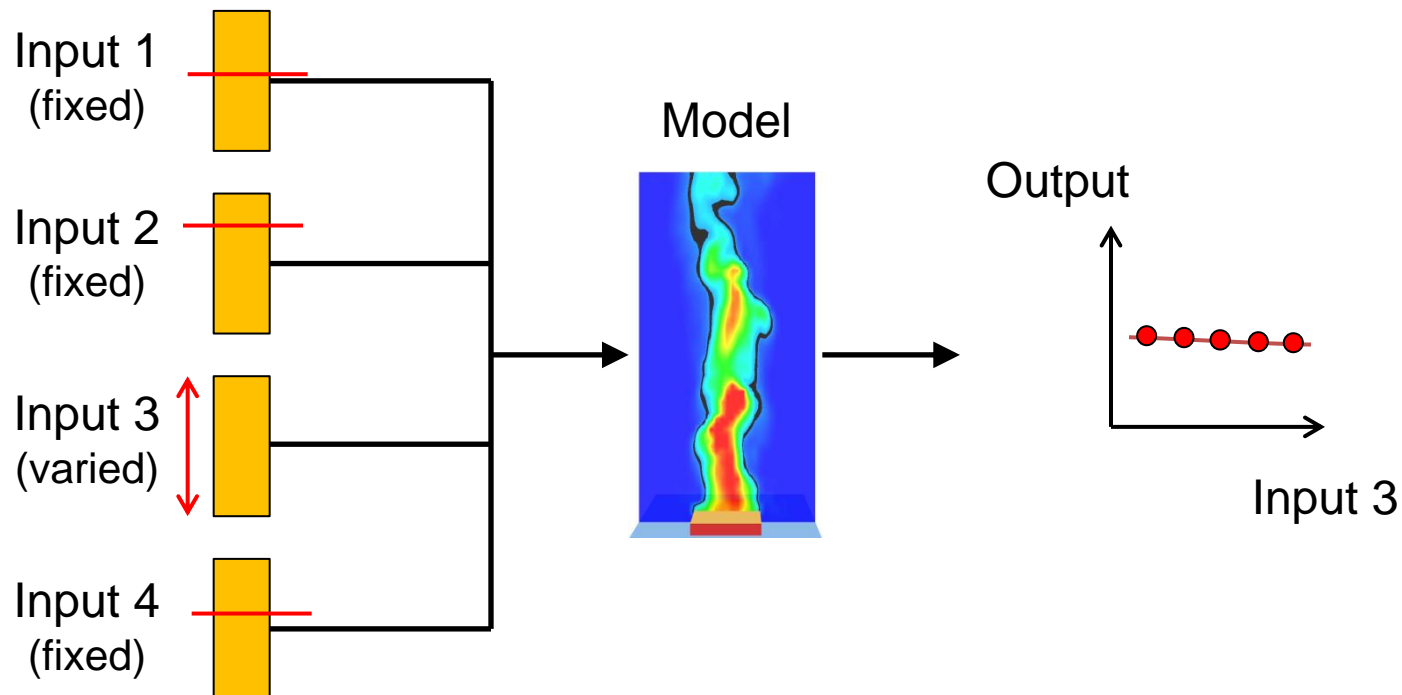
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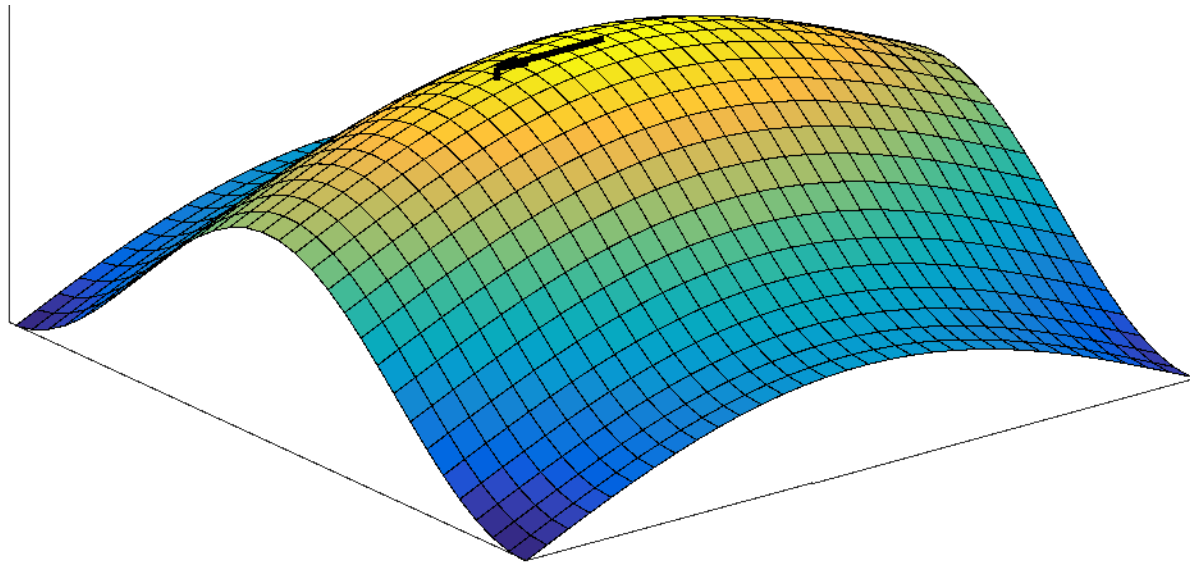
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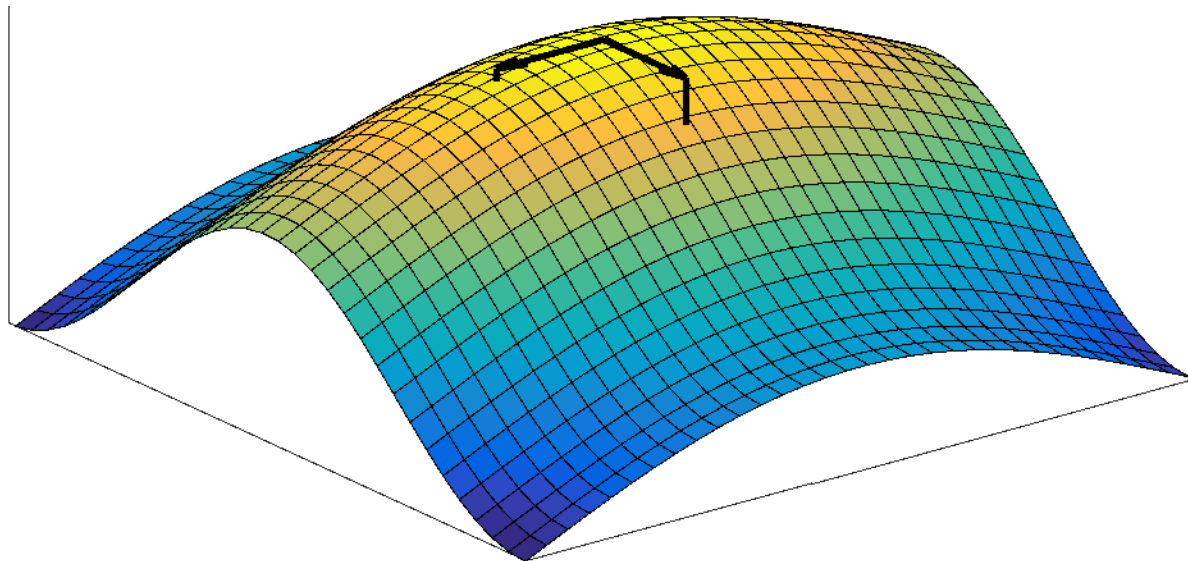
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- Limitations:
 - No information provided on interactions between inputs

Sensitivity Analysis

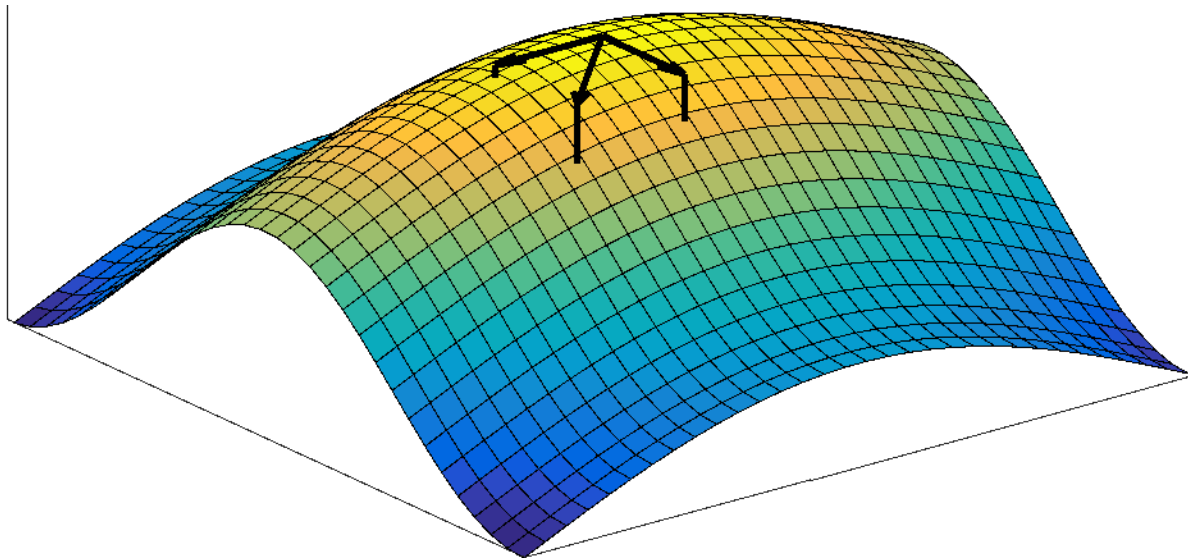
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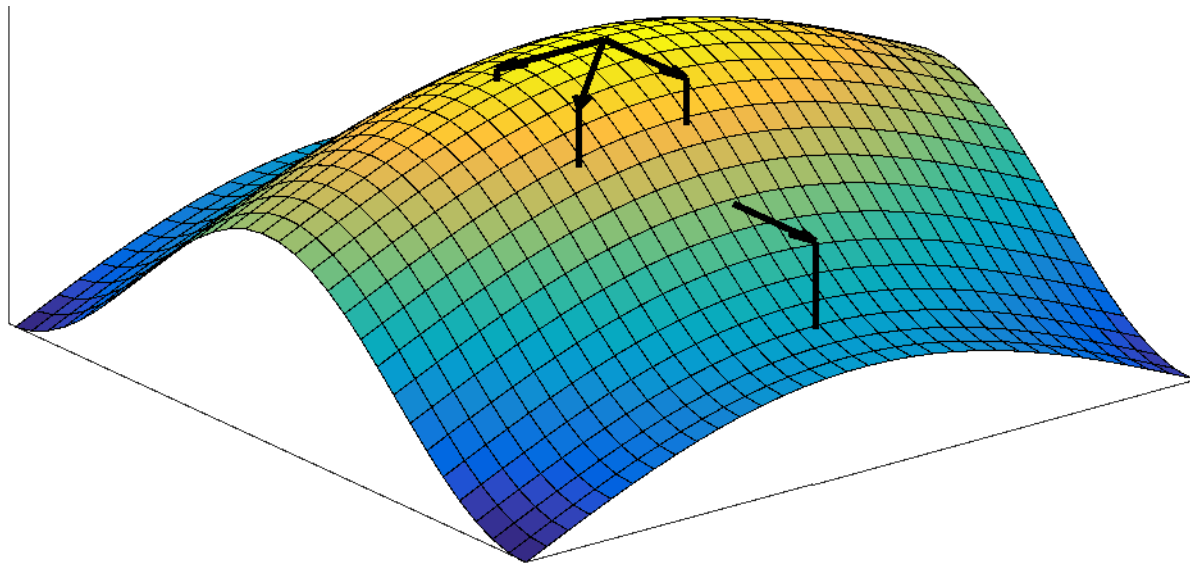
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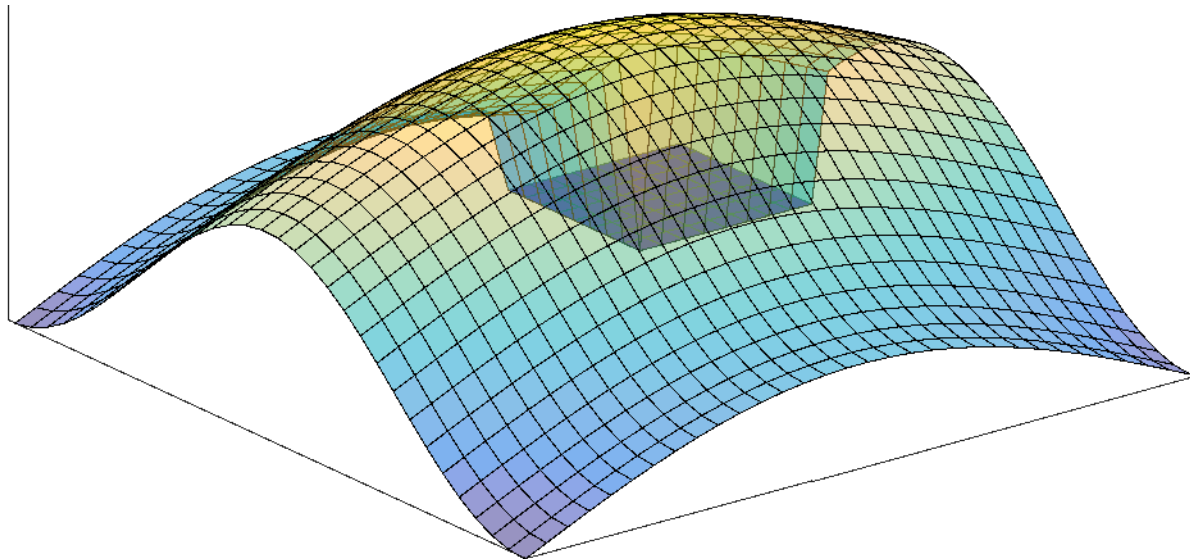
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 - Results depend upon choice of baseline

Sensitivity Analysis

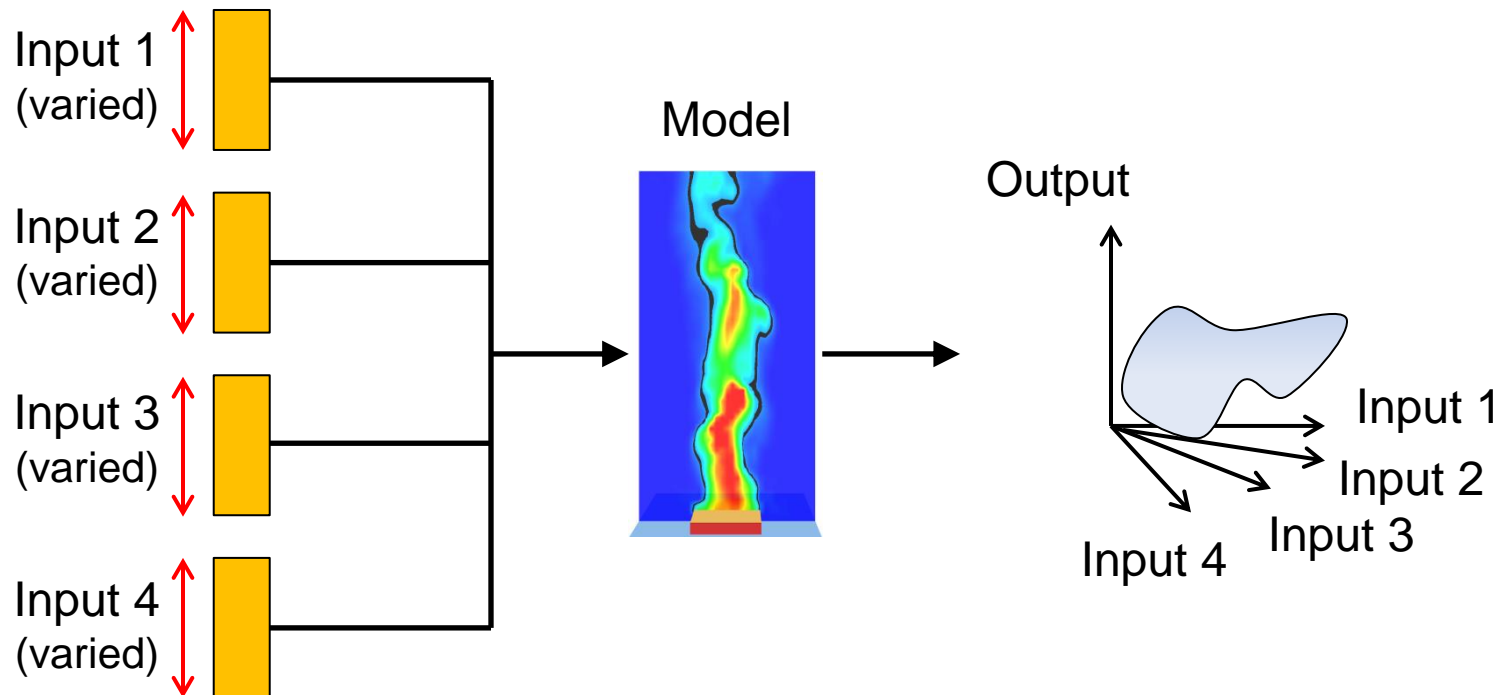
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- Limitations:
 - No information provided on interactions between inputs
 - Results depend upon choice of baseline
 - Analysis may miss important effects (e.g. cliff edges)

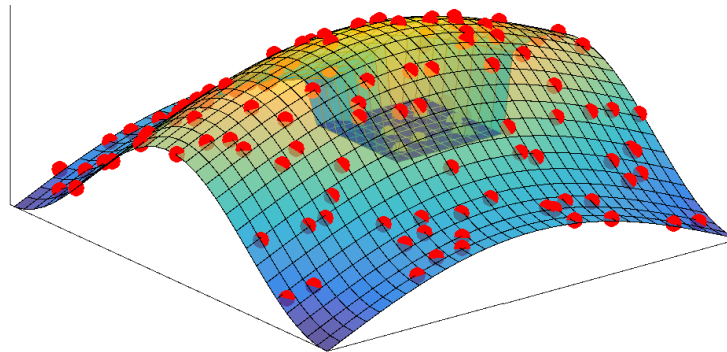
Sensitivity Analysis

- Two approaches for sensitivity analysis:
 1. **Local:** vary one parameter at a time from a “baseline” case
 2. **Global:** vary all parameters simultaneously



Sensitivity Analysis

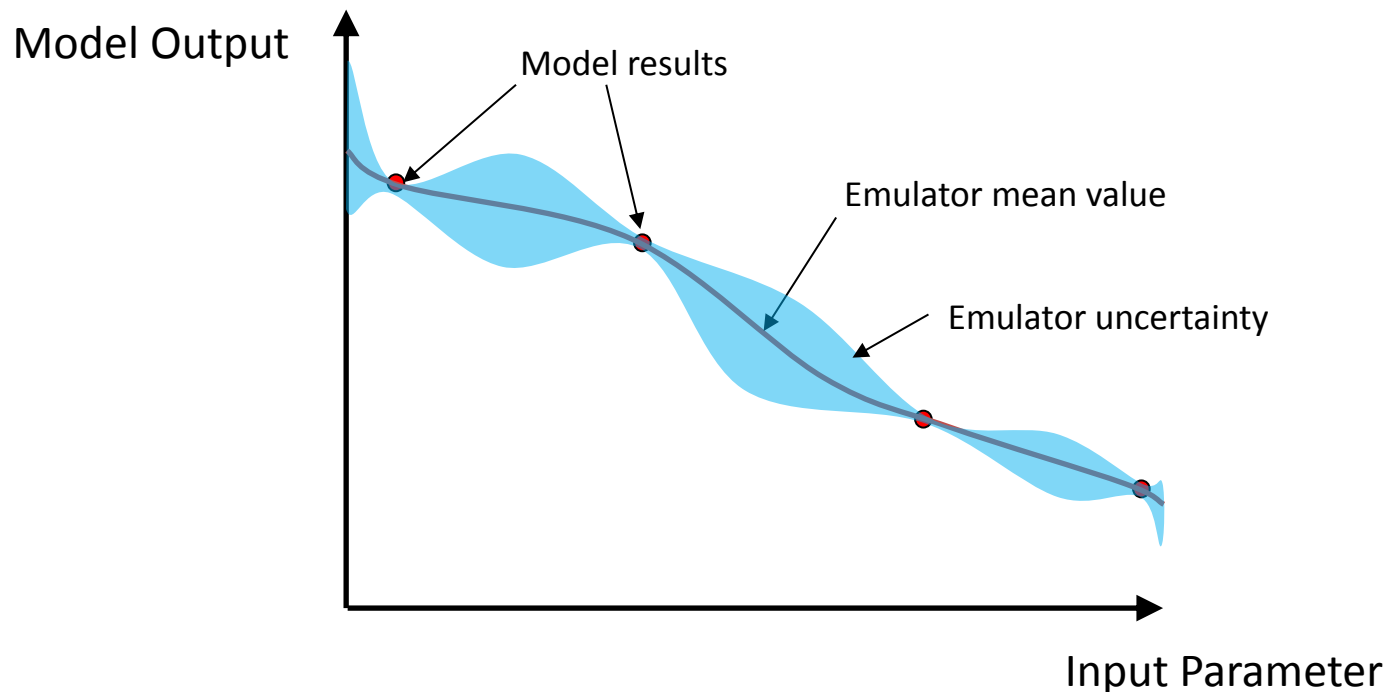
- Two approaches for sensitivity analysis:
 1. **Local:** vary one parameter at a time from a “baseline” case
 2. **Global:** vary all parameters simultaneously



- Benefits:
 - Results do not depend upon choice of baseline
 - Information provided on interactions between inputs
- Problem:
 - Many thousands of model calculations required to cover combinations of all inputs
 - Computing time can be prohibitive

Solution: emulators

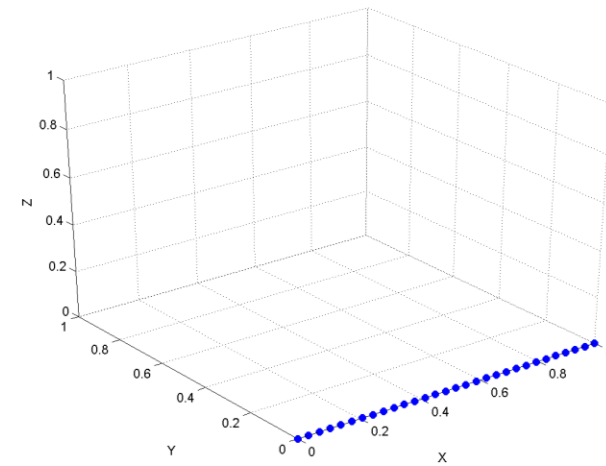
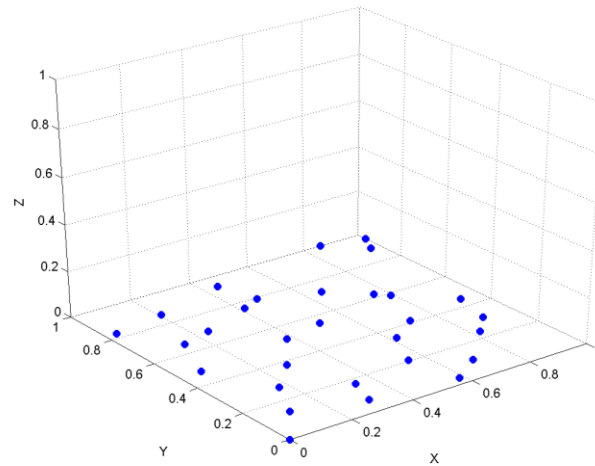
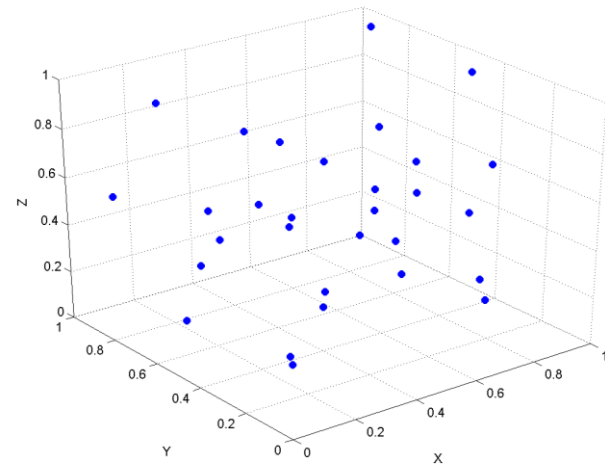
- Fit a statistical emulator to a few hundred model results
- Run the sensitivity analysis using the emulator (much faster)



- Underlying assumption of emulator: output is a smooth, continuous function of the input parameters

Maximin Latin Hypercube

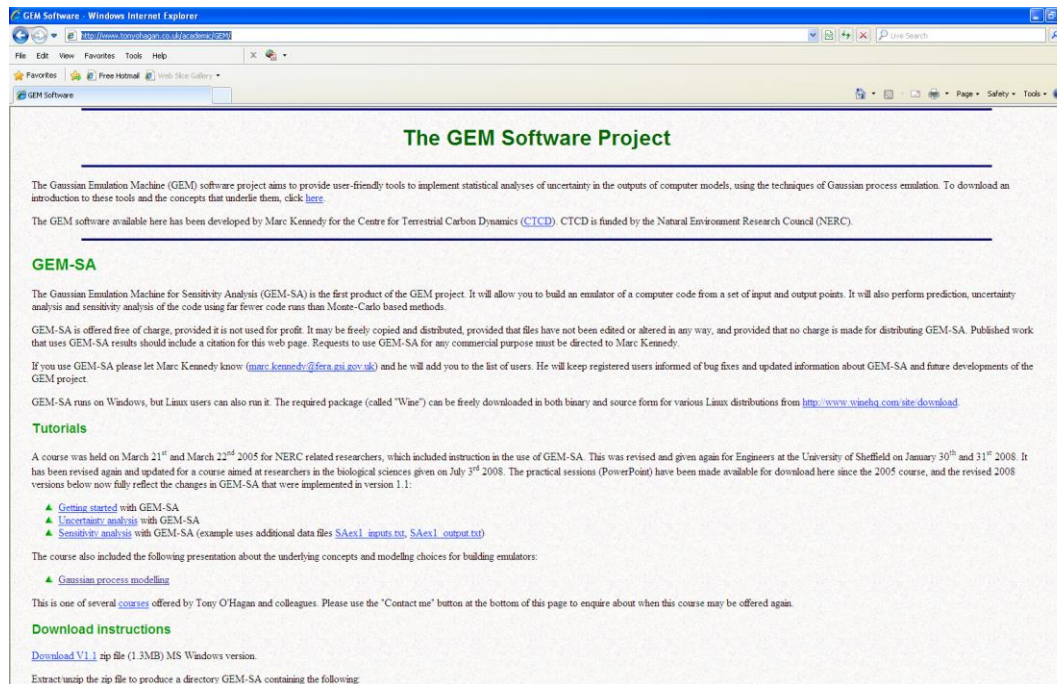
- Example: 3 input variables, 30 samples



- If Parameters Y and Z had no effect on the results, all 30 samples are equispaced across Parameter X sample space
- Often, just 1 or 2 input parameters dominate model predictions : Latin hypercube maximises coverage from limited number of points

Sensitivity Analysis: GEM

- Gaussian Emulation Machine (GEM)
- Free software (for non-commercial use) developed by Marc Kennedy and colleagues at Sheffield University
<http://www.tonyohagan.co.uk/academic/GEM/>



Example: CO₂ release

- Which of these inputs (or combinations of inputs) has a significant effect on the results?

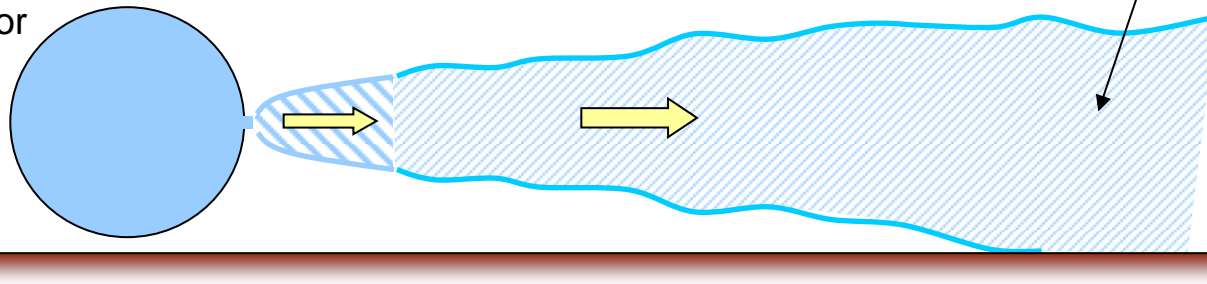
Sample Inputs:

1. Reservoir temperature: 5 – 30 °C
2. Reservoir pressure: 100 – 150 barg
3. Orifice size: ½ – 2 inch
4. Wind speed: 0.5 – 50 m/s
5. Ambient humidity: 0 – 100% RH
6. Ground roughness: 0.0001 – 1 m
7. Release height: 0.5 – 3 m

Output of interest:

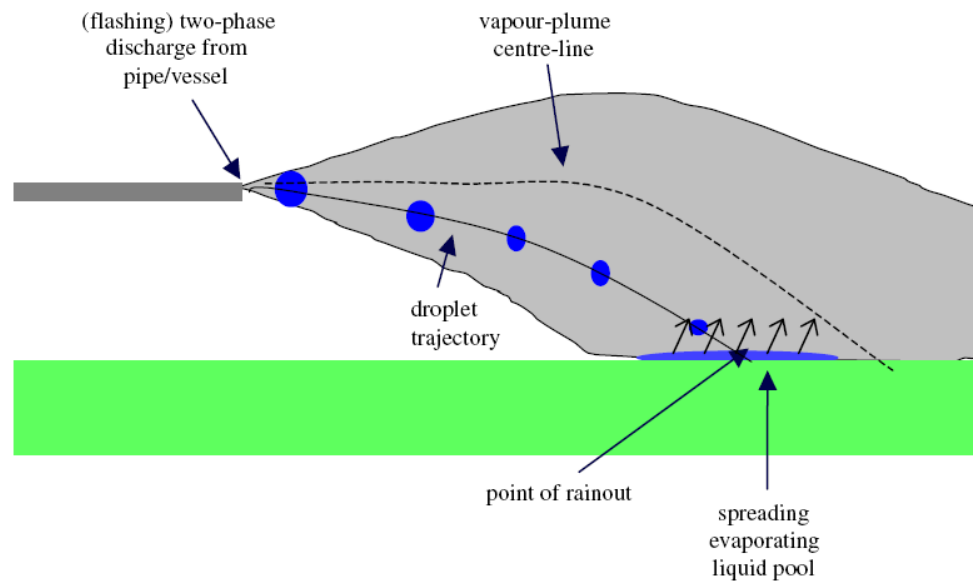
“Dispersion distance” where concentration reaches 6.9% v/v CO₂

Leak from above-ground vessel or large pipe



Consequence model: Phast

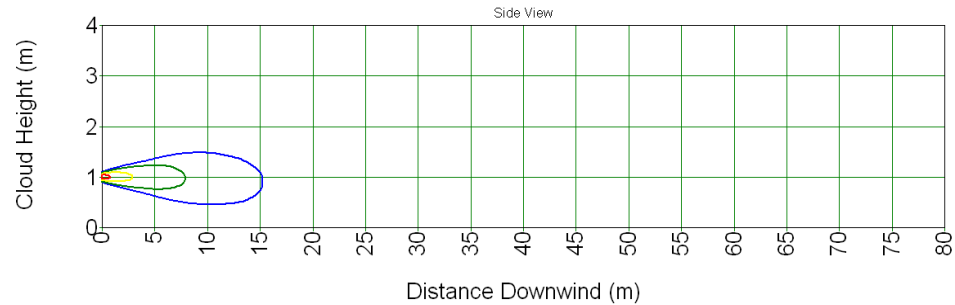
- Integral release and dispersion model produced by DNV-GL Software
- Validated against CO₂ dispersion experiments conducted by Shell and BP



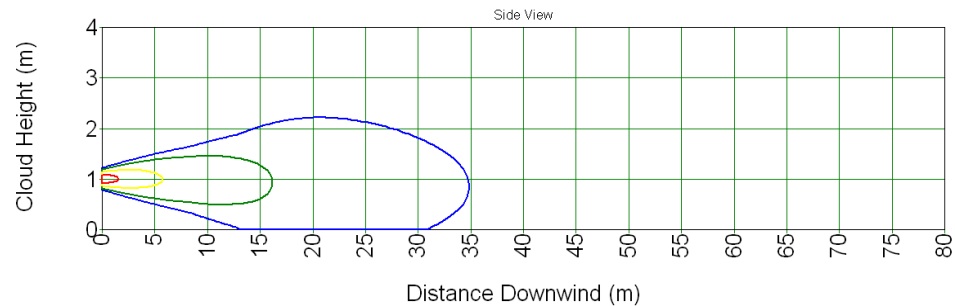
Phast results

Orifice
diameter

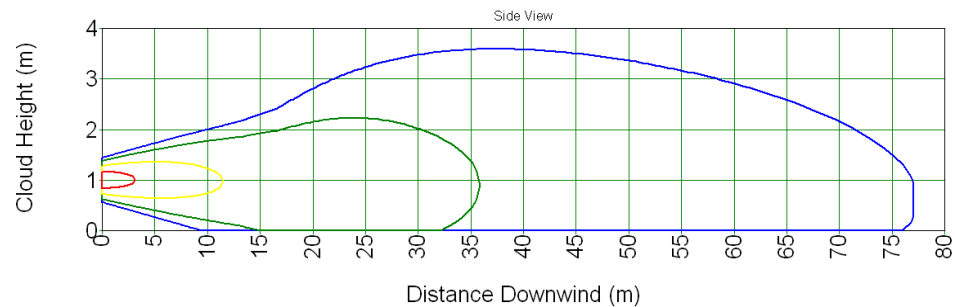
½ inch



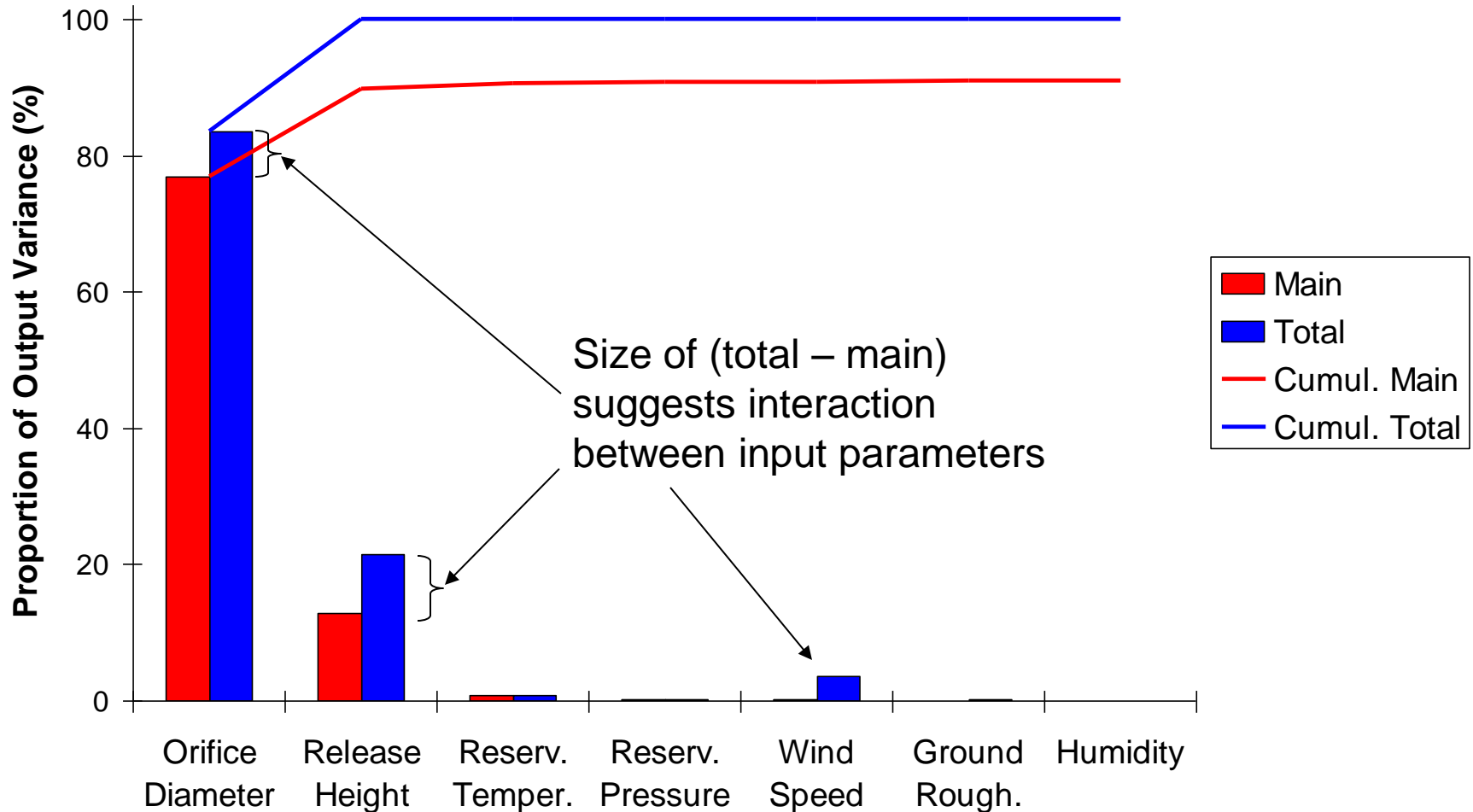
1 inch



2 inch

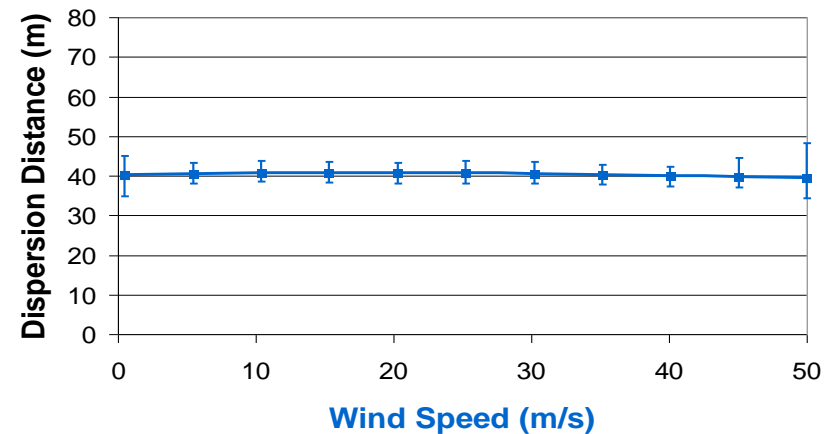
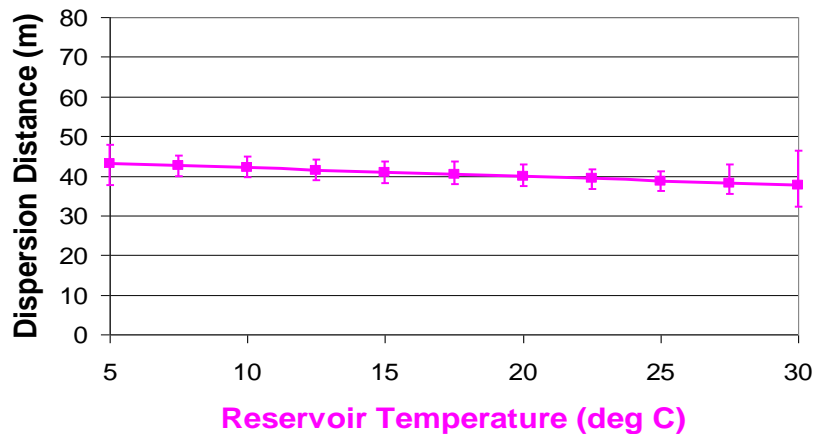
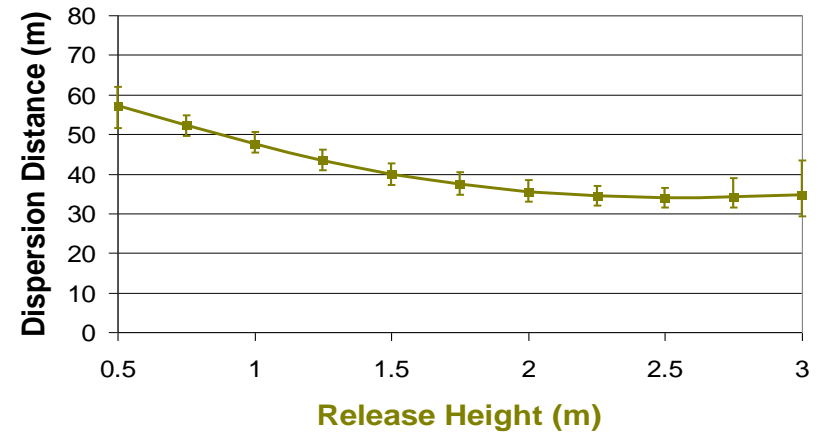
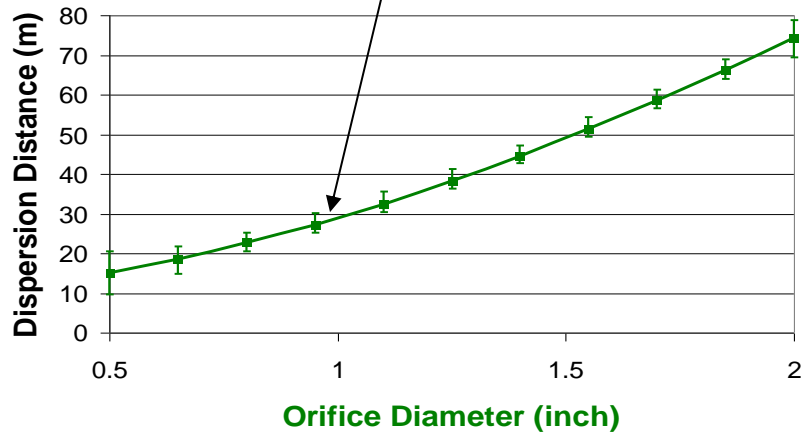


Sensitivity analysis results

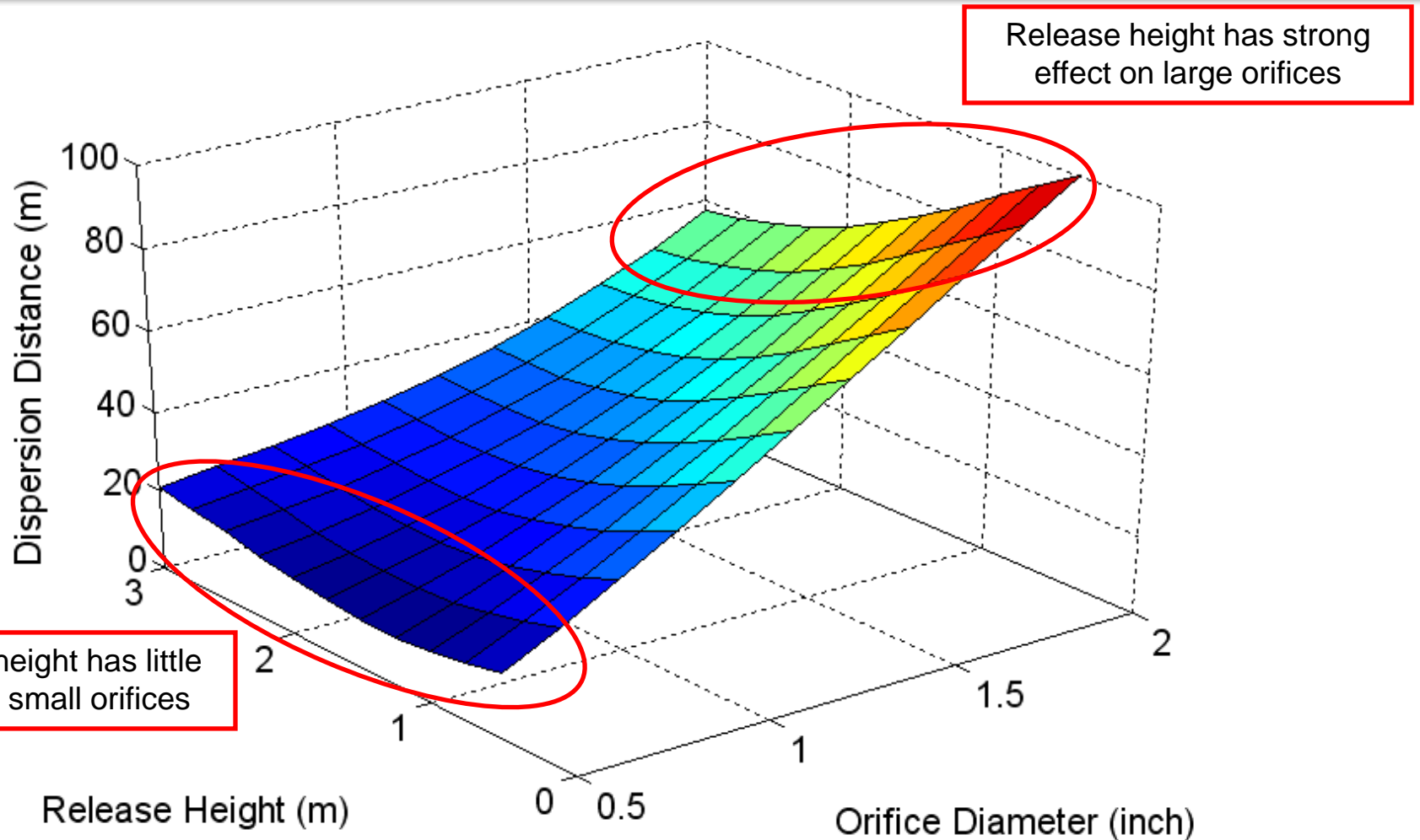


Model behaviour

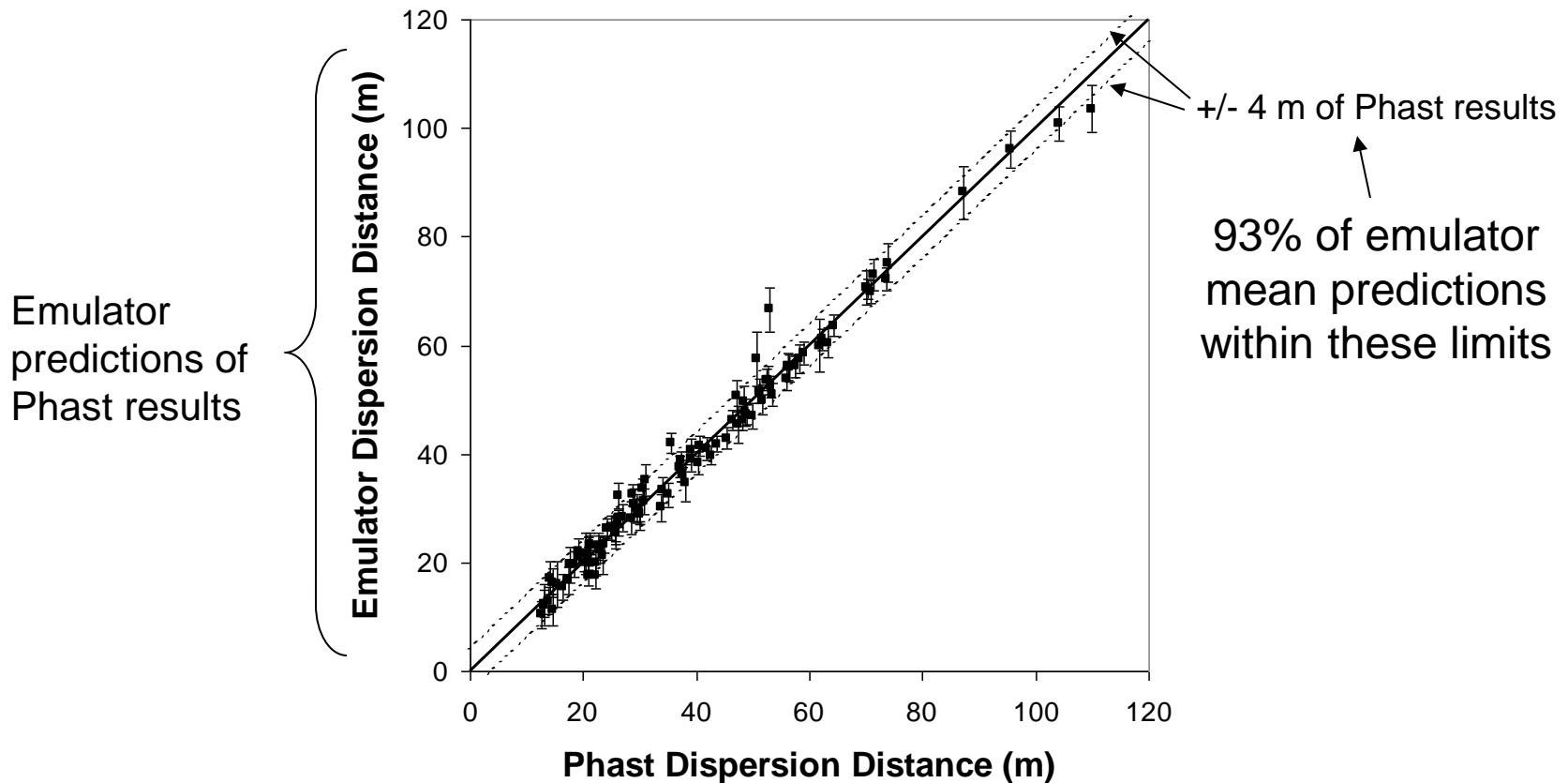
e.g. fix orifice diameter at 1 inch and average over range of all other input parameters



Joint effects



Emulator cross-validation



- Adequate accuracy for the purposes of identifying model trends
- Analysis repeated with 400 Phast runs gave similar results

Example: LNG pool fires

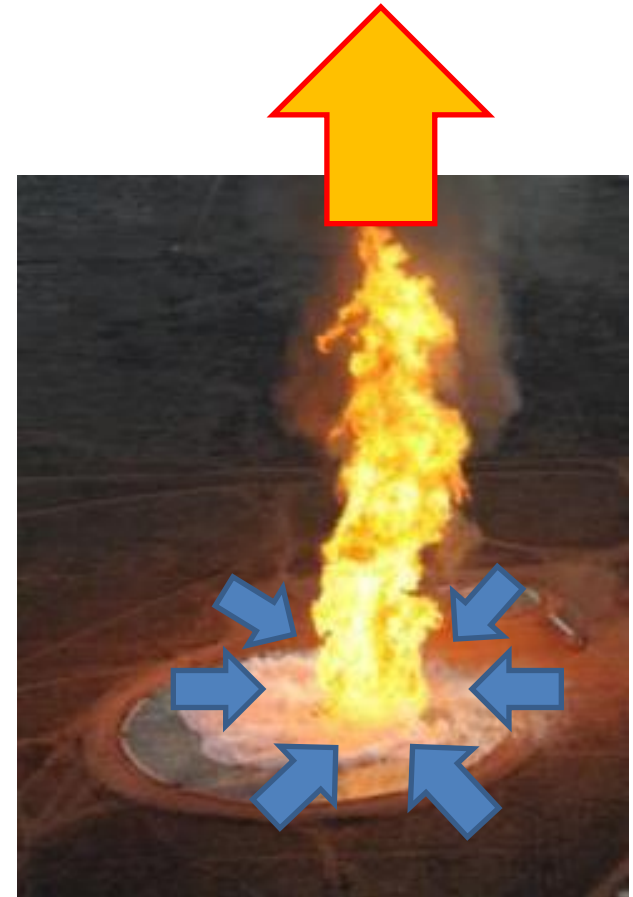
- Phoenix large-scale LNG pool fire experiments conducted by Sandia National Laboratories in 2009
- Two tests involved ignited LNG spills on water
 - 21 m diameter LNG pool
 - 83 m diameter LNG pool
- 83 m pool - unexpected results
 - Fire did not extend across LNG pool surface
 - Fire significantly higher than predicted
 - Very little smoke



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<http://prod.sandia.gov/techlib/access-control.cgi/2010/108676.pdf>

LNG pool fires: Background

- Hypothesis (proposed by Shell Research Ltd)
 - Strong thermal updraft from large fire
 - High speed inwards flow of air/vapor into the base of the fire
 - Flames unable to spread outwards from central ignition location
- Video analysis
 - 2-3 m/s flow into base of fire
 - Sufficient to arrest flame spread?
- Investigation at HSL funded by Shell Research Ltd
 - CFD modelling
 - Flame spread experiments
- Sensitivity analysis funded by HSE

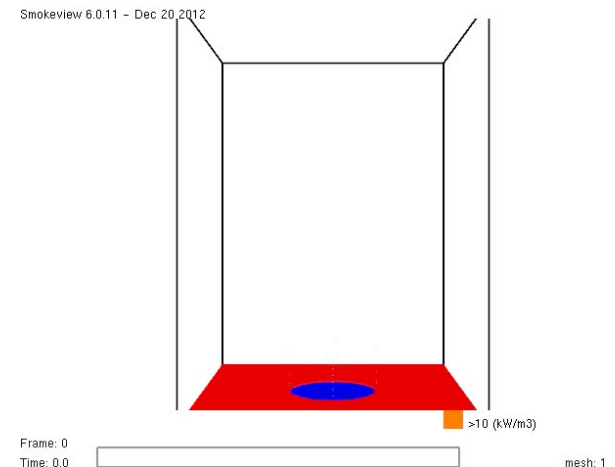
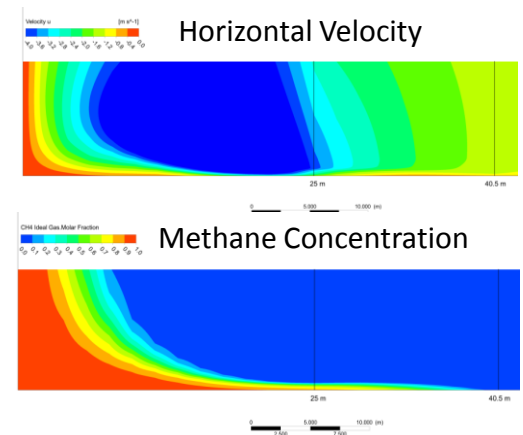


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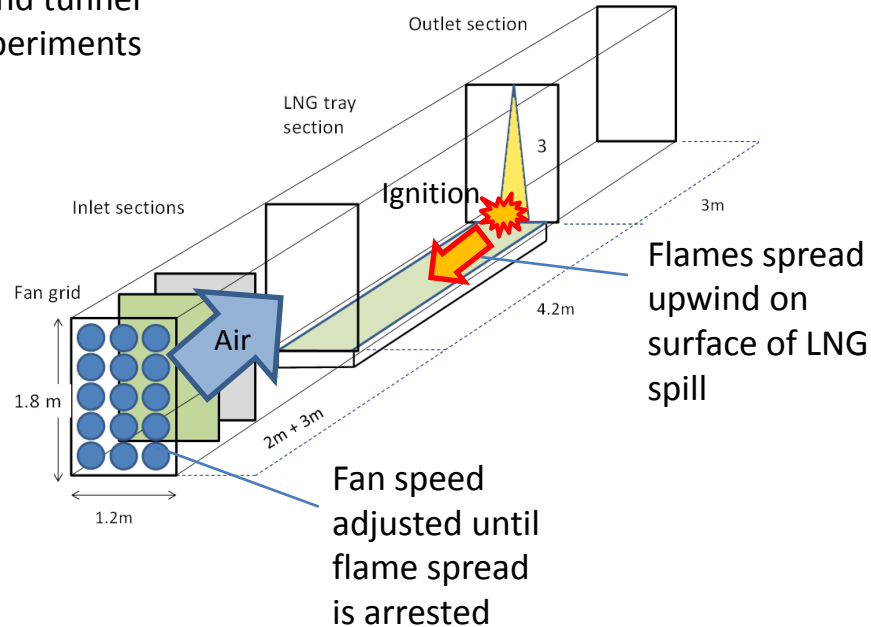
LNG pool fires: Modelling

- CFD modeling aim
 - To predict the speed of air/vapour entrained into the base of the fire in the Phoenix test
- CFD models tested
 - Ansys-CFX: volumetric heat source
 - FDS: combustion model
- Speed of entrained air/vapour flow
 - Ansys-CFX = 3.7 m/s
 - FDS = 3.2 m/s
- Phoenix test provides only one data point



LNG pool fires: Experiments

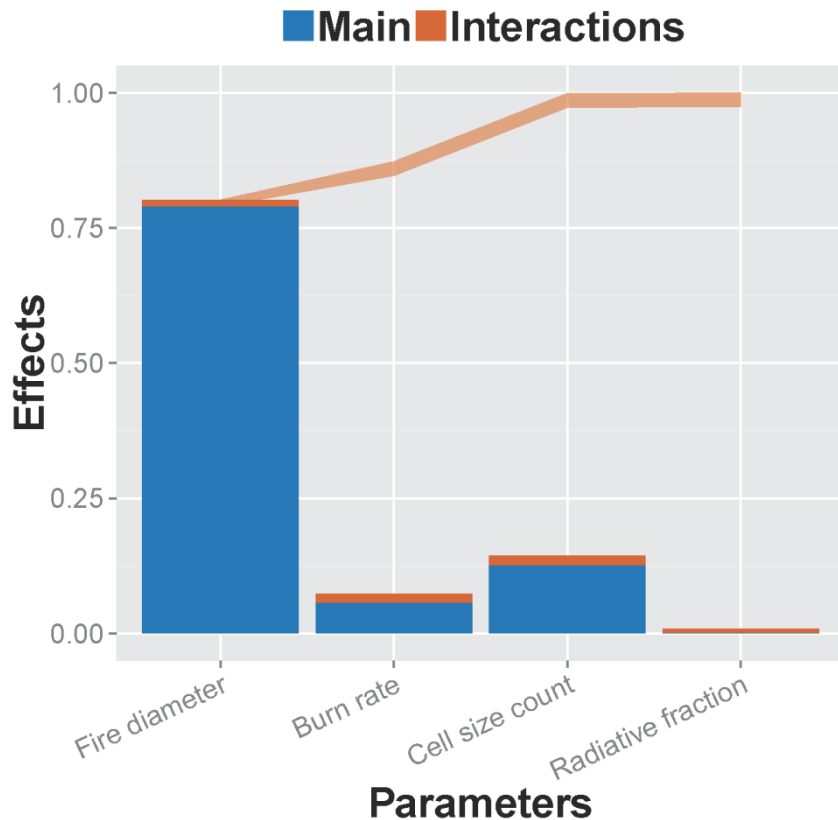
Wind tunnel experiments



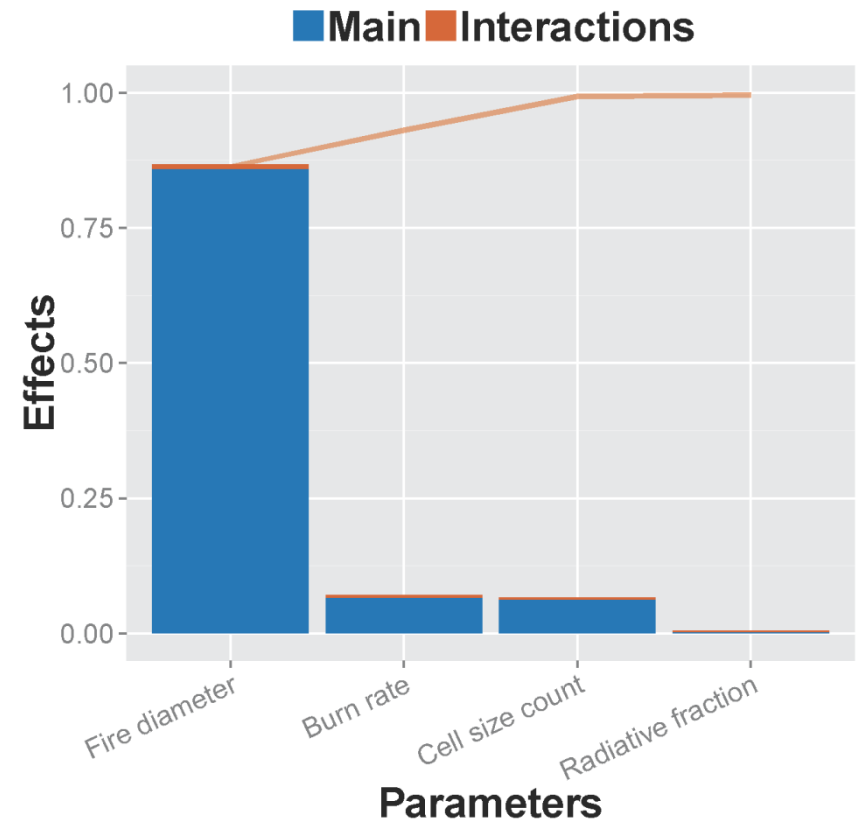
■ Main findings

- Flame stabilised when air flows were 2.8 and 3.2 m/s
- Flame progressed further along low speed areas adjacent to walls
- Stabilised conditions equated to turbulent flame speed of 2 m/s

LNG pool fires: Entrainment velocity sensitivity analysis

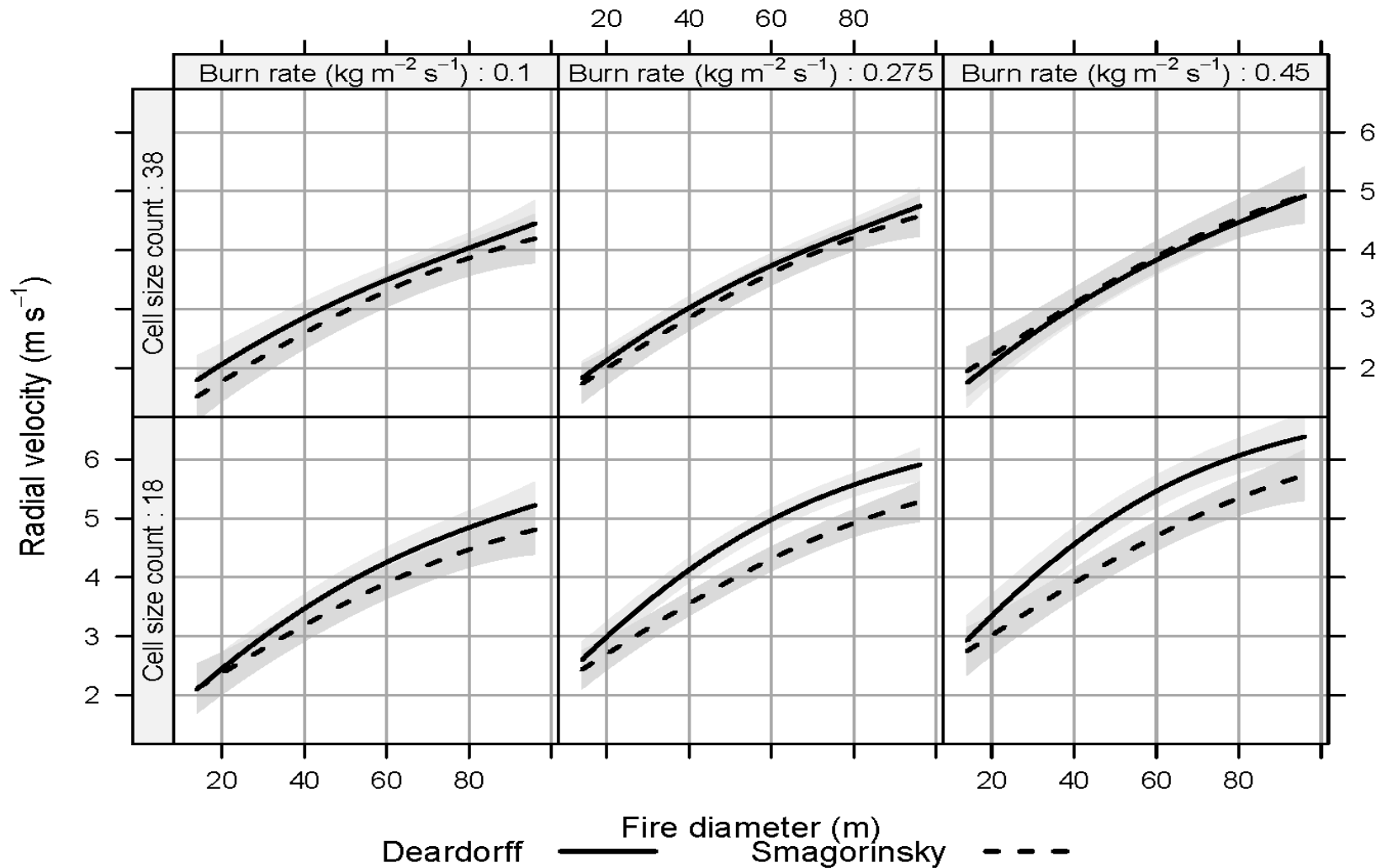


Deardorff turbulence model



Smagorinsky turbulence model

LNG pool fires: Entrainment velocity model behaviour

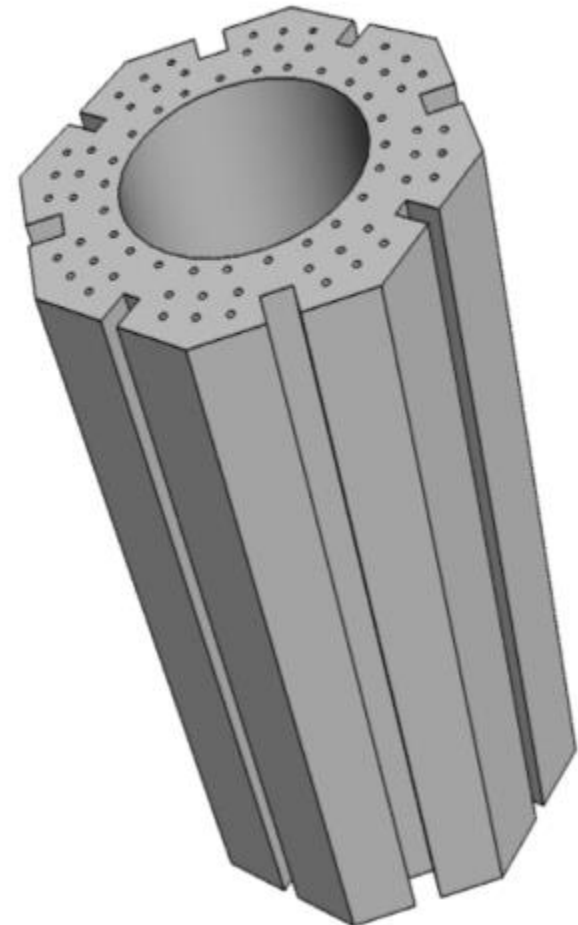


LNG pool fires: Sensitivity analysis

- Pool diameter had greatest influence on entrainment velocity
- Burn rate had only minor effect on entrainment
- Turbulence model predictions converged on finer mesh
- Inwards flow of air/vapour exceeds 2 m/s when pool diameter > 20 m

AGR graphite bricks

- Graphite properties change due to radiation
- Limited data available, collected during shutdowns
 - Inspection
 - Sampling
- Finite element modelling of graphite bricks
- Emulator used to perform Global Sensitivity Analysis of FE model

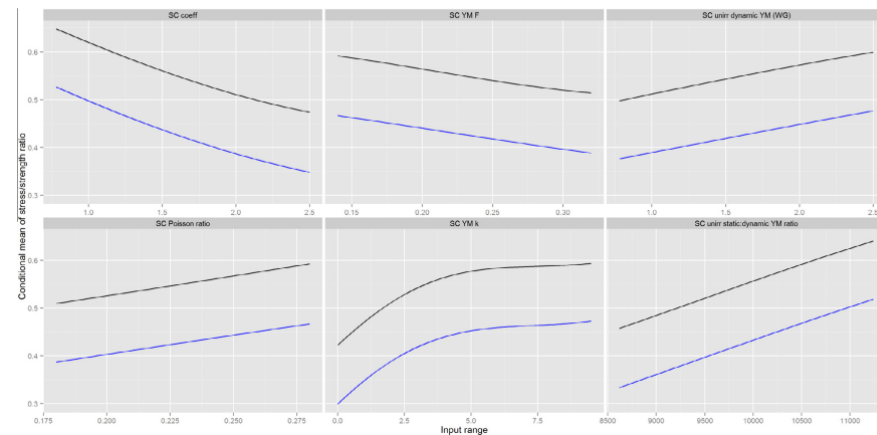


AGR graphite bricks

- 20 uncertain parameters, 100 simulations
- 6 influential parameters
- Main effects of 6 influential parameters

Main and total effect sensitivity indices for the 20 input parameters in the experiment. Results are based on an analysis of outputs at 10fpy for the at power and shutdown conditions.

Parameter	Power (10 fpy)		Shutdown (10 fpy)	
	Main effect	Total effect	Main effect	Total effect
Primary creep coefficient	0.0001	0.0005	0.0001	0.0005
Primary creep Poisson's ratio	0.0000	0.0000	0.0000	0.0000
Primary creep Young's modulus weight loss fitting constant F_i	0.0019	0.0093	0.0018	0.0092
Primary creep Young's modulus weight loss fitting constant k_i	0.0057	0.0136	0.0058	0.0137
Primary creep Unirradiated dynamic Young's modulus (WG)	0.0011	0.0016	0.0011	0.0016
Primary creep Unirradiated dynamic Young's modulus (AG)	0.0000	0.0000	0.0000	0.0000
Primary creep Unirradiated static to dynamic Young's modulus ratio	0.0002	0.0023	0.0002	0.0023
Primary creep Irradiated dynamic Young's modulus amplitude term a	0.0000	0.0000	0.0000	0.0000
Primary creep Irradiated dynamic Young's modulus location term b	0.0000	0.0001	0.0000	0.0000
Primary creep Unirradiated Shear modulus	0.0000	0.0000	0.0000	0.0000
Secondary creep coefficient	0.2310	0.2474	0.2319	0.2489
Secondary creep Poisson's ratio	0.0535	0.0628	0.0537	0.0629
Secondary creep Young's modulus weight loss fitting constant F_i	0.0421	0.0857	0.0418	0.0852
Secondary creep Young's modulus weight loss fitting constant k_i	0.2094	0.2763	0.209	0.276
Secondary creep Unirradiated dynamic Young's modulus (WG)	0.0739	0.0808	0.0735	0.0804
Secondary creep Unirradiated dynamic Young's modulus (AG)	0.0000	0.0000	0.0000	0.0000
Secondary creep Unirradiated static to dynamic Young's modulus ratio	0.2825	0.3011	0.2823	0.3009
Secondary creep Irradiated dynamic Young's modulus amplitude term a	0.0003	0.0017	0.0003	0.0017
Secondary creep Irradiated dynamic Young's modulus location term b	0.0056	0.0175	0.0056	0.0175
Secondary creep Unirradiated Shear modulus	0.0008	0.0058	0.0008	0.0058



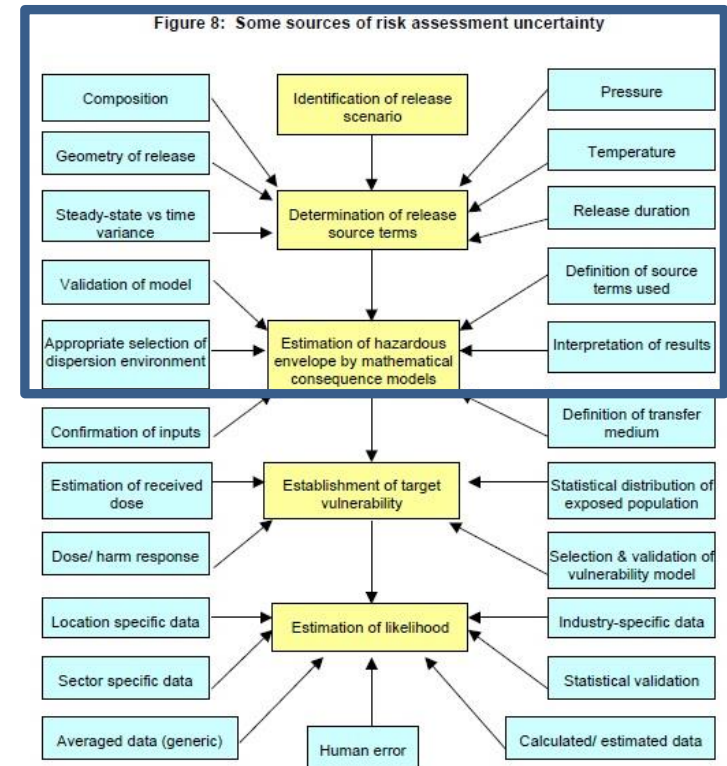
<http://dx.doi.org/10.1016/j.nucengdes.2016.09.007>

Conclusions

- Global sensitivity analysis can identify important parameters and provide useful understanding of model behaviour
- Emulator-based approach can be used for practical engineering calculations at low cost
 - Phast CO₂ dispersion simulations and analysis took less than 30 minutes on a laptop
- In principle, these methods are applicable to other models and types of inputs, e.g. QRA

Future work

- Joint industry project on sensitivity and uncertainty analysis for QRA
 - Consequence modelling
 - Probabilistic modelling



Guidance on Risk Assessment for Offshore Installations
Offshore Information Sheet No. 3/2006

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